

Water Quality and Potential Sediment Erosion Assessment for Proposed Construction at Fort Knox, Kentucky

Steven L. Ashby, William D. Martin, and Cassandra N. Gaines

February 2001

20010426 070

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products.

The findings of this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.



Water Quality and Potential Sediment Erosion Assessment for Proposed Construction at Fort Knox, Kentucky

by Steven L. Ashby

Environmental Laboratory U.S. Army Engineer Research and Development Center 3909 Halls Ferry Road Vicksburg, MS 39180-6199

William D. Martin, Cassandra N. Gaines

Coastal and Hydraulics Laboratory U.S. Army Engineer Research and Development Center 3909 Halls Ferry Road Vicksburg, MS 39180-6199

Final report

Approved for public release; distribution is unlimited

Contents

Preface	iv
Introduction	1
Background	1
General Description of Proposed Sites	2
Cedar Creek Range	2 2 2
Methods	3
Results	4
Summary	8
Tables 1-9	
Figures 1-17	
References	25
Appendix A—Minimum and Maximum Values for Selected Water Quality Constituents in the STORET Database	A 1
Appendix B—Data from the Kentucky Division of Water Monitoring Program	В1
Appendix C—Output from FLUX Applications for the Salt River and Rolling Fork River Calculation of Loading Estimates for Total Nonfilterable Residue Concentrations	C1
SF 298	

Preface

The work reported herein was conducted for the U.S. Department of the Army, Fort Knox, KY, by the U.S. Army Engineer Research and Development Center (ERDC) under the purview of the Environmental Laboratory (EL) and the Coastal and Hydraulics Laboratory (CHL). Funds for this study were provided under the Military Interdepartmental Purchase Request Number MIPR0KDDK00020.

This report was prepared by Dr. Steven L. Ashby, Environmental Processes and Engineering Division (EPED), EL, and Dr. William D. Martin, Watershed System Group, Modeling Systems Branch, Estuaries and Hydroscience Division, and Ms. Cassandra N. Gaines, Watershed Systems Group, CHL. Preparation of this report was under the general supervision of Dr. Richard E. Price, Chief, EPED, Dr. John W. Keeley, Acting Director, EL, and Mr. David R. Richards, Chief, Modeling Systems Branch, and Dr. Thomas W. Richardson, Acting Director, CHL.

At the time of publication of this report, Dr. James R. Houston was Director of ERDC, and COL James S. Weller, EN, was Commander.

This report should be cited as follows:

Ashby, S. L., Martin, W. D., Gaines, C. N. (2001). "Water quality and potential sediment erosion assessment for proposed construction at Fort Knox, Kentucky," ERDC SR-01-1, U.S. Army Engineer Research and Development Center, Vicksburg, MS.

Introduction

New training facilities proposed for construction at the Fort Knox Northern Training Complex (NTC) include a digital training range and a complex of drop/landing zones and maneuver area (DLZMA) and are depicted in Figure 1. Three alternatives exist for the digital training range, one at the Yano range, one at the Cedar Creek range, and one at the Wilcox range site. The drop and landing zones and maneuver areas have been proposed for construction near the Mounted Urban Combat Training Area (MUCT) near the Wilcox range site.

Concerns expressed during review of the Environmental Assessments were focused on the potential for adverse impacts to water quality and aquatic resources due to increased sediment erosion associated with construction and subsequent use of these facilities. Consequently, an assessment of the existing water quality and the potential for adverse impacts was conducted for an Environmental Impact Statement (EIS) currently in preparation. The objective of this assessment was to compile and evaluate applicable water quality and flow data for describing existing conditions and evaluating potential impacts associated with the proposed construction. Biological evaluations of aquatic resources have been assessed in separate studies.

Background

Major surface waters in the study area include the Salt River and Rolling Fork River. Smaller tributaries to these two rivers in the area include, Mill Creek, Plum Creek, Wilson Creek, Long Lick Creek, Elm Creek, Brier Creek, Cox Creek, Brooks Run, Floyds Fork, Cedar Creek, and Brushy Fork. Additional small rivers and creeks occur in the area and several lakes and ponds exist including Duck Lake, Wilcox No. 3 Lake, Wilcox Lake, and Pearl Pond, which are in or near the proposed Wilcox site. The small streams are typically sloped from 3 to 7%, with cobble substrate low in areas of accumulation of fine sediment. A more complete description of low order streams and lakes in the study area are provided in Payne and Green (2001). Water supply in the vicinity of Fort Knox and downstream is from groundwater.

The Salt River Watershed is drained by 3,770 miles of rivers and streams but only 650 miles (17%) have been assessed for water quality standards for swimming and fishing. Major pollutant concerns in areas with large populations are related to urban runoff and discharges from wastewater treatment facilities, industries, and septic tanks. Pollutants of concern include bacteria and pathogens, silt, metals, chorine, pesticides, and organic chemicals. In more rural settings, pollutants of concern include silt, animal waste, nutrients and pesticides. Rapid population growth and urban sprawl is a priority concern in the watershed since these activities are major contributors to increased surface runoff and pollutant loading. Since 1990, the population of Bullitt County increased 20-24% and fewer than 50% of the households have access to public treatment facilities. Most of the counties do not have adequate zoning laws or local ordinances or staff to adequately protect water quality (Kentucky Division of Water publication (KDW), 1998). The Lower Salt River watershed begins at Taylorsville Lake Dam and flows to the Ohio River at West Point. Floyds Fork, Rolling Fork, and Cox Creek are major tributaries to the Lower Salt River. The principal land use activity is agriculture (61%) followed by forest (24%), then residential (9%), and urban (5%). The Lower Salt River and its tributaries are located in an area that was historically a swamp. Due to the increased population and changes in land use, this area has flooding and drainage problems (KDW 1998). Soils in the study area have a medium to high potential for sediment runoff, slow to moderate infiltration and can be classified primarily in the McGary, Markland, Lawrence, Garmon, Crider, and Baxter Associations.

Several rivers and streams in the lower Salt River basin have been evaluated for water quality problems (KDW 1998). The Lower Salt River downstream from Shepherdsville is designated as poor but the designation changes to good where the Rolling Fork joins the river. A thorough ecological assessment of the Lower Salt River watershed has not yet been done (KDW 1998). In Bullitt County, the Salt River, Cedar Creek, and Rolling Fork have been classified as impaired for swimming due to pathogens. Cox Creek in Bullitt County has been assessed as having water quality problems, primarily excessive nutrients and siltation and is classified as impaired for aquatic life. Brooks Run in Bullitt County has been classified as impaired for swimming and aquatic life attributed to pathogens and low dissolved oxygen concentrations as a result of organic enrichment. Pennsylvania Run has also been classified as impaired for swimming and aquatic life due to low dissolved oxygen concentrations as a result of organic enrichment. Floyds Fork has also been classified as impaired for swimming and aquatic life due to pathogens, nutrients, and low dissolved oxygen concentrations as a result of organic enrichment. Wilson Creek meets standards for swimming and aquatic life.

In Hardin County, Brushy Fork has been classified as impaired for swimming due to pathogens and Mill Creek has been classified as impaired for aquatic life due to metals, ammonia (unionized), and low dissolved oxygen concentrations as a result of organic enrichment. The Salt River meets standards for swimming and aquatic life in Hardin County. There has not been a similar water quality evaluation of the Rolling Fork River.

General Description of Proposed Sites

Cedar Creek Range – Utilization of this site would require extensive excavation of adjacent hills and likely result in considerable increase in sediment erosion. The site is approximately 12.5 miles from the Mounted Urban Combat Training Area (MUCT) and the proposed drop/landing zones and maneuver area (DLZMA), with no direct route available through Fort Knox territory. To get to the MUCT, tanks would have to be hauled off post and through congested areas or a new road would have to be established on the post. Building an onpost road is possible but would require transiting an impact area. Potential environmental impacts related to vegetation removal and increased sediment erosion would likely be caused by on-post road construction to connect the Cedar Creek range to the MUCT.

Yano Range – This site could be modified to include the digital training range with minimal environmental impacts. The site is approximately 12.5 miles from the MUCT and proposed DLZMA, with no direct route available through the Fort Knox territory. As required for the Cedar Creek Range, to get to the MUCT and proposed DLZMA, tanks would have to be hauled off post and through congested areas or a new road would have to be established on the post. Building an on-post road is possible but would require transiting an impact area. Potential environmental impacts related to vegetation removal and increased sediment erosion would likely be caused by on-post road construction to connect the Yano range to the MUCT and proposed DLZMA.

Wilcox Range - Utilization of this site would require extensive clearing of forested areas that include wetlands and lakes. The area also contains habitat for endangered species that would be adversely impacted. Potential environmental impacts include increased sediment erosion, loss of habitat, and loss of wetlands. This site is located closest (1-3 mi) to the MUCT and proposed DLZMA and would require much less construction to be connected than the Cedar Creek or Yano ranges.

The DLZMA (Areas 1-5, and 9) contain approximately 1,171 acres. The vast majority of this land is forested. There are numerous sinkholes associated with the karst topography in the area that would possibly receive runoff and sediments associated with construction of the DLZMA. Removal of forest vegetation to accommodate training needs associated with the DLZMA will potentially increase runoff and sediment/material transport, particularly during construction. Establishment of buffer zones has been proposed to reduce the impact of materials transported with runoff to the sinkholes and nearby surface waters.

Methods

Discharge information on area creeks, streams, and rivers was retrieved from the US Geological Survey (USGS) water resources website (http://waterdata.usgs.gov/nwis-w/KY/) and from the US Army Engineer District in Louisville, KY. Water quality data were retrieved from the US Environmental Protection Agency (EPA) database (Storage and Retrieval System (STORET)), and requested from the Kentucky Department of Environmental Protection (KDEP), Division of Water and the Fort Knox database for the Kentucky Pollutant Discharge Elimination System (KPDES) permit for the facility. Water quality data for the city of West Point, which is near the confluence of the Salt River and the Ohio River, was included in the retrieval from STORET.

Discharge data for the two major rivers in the study area (the Salt River and Rolling Fork River) were plotted and general temporal trends were described. Water quality values of selected chemical constituents collected by the KDEP were compared for both rivers and general temporal trends were described. Estimates of annual loads of total nonfilterable residue (TNFR), or suspended solids, were calculated with discharge data for the Salt River at Shepherdsville, KY and the Rolling Fork River at Boston, KY and TNFR data collected monthly in the period from October 1995 to December 1998 by the KDEP. Water quality data from other sources had limited recently collected data and consequently were tabulated for subsequent discussion. A suite of regression models (FLUX) developed by Walker (1996) was used to calculate the estimates of TNFR loads for each river. Use of FLUX provides statistical comparisons of six different regression techniques to determine the best fit for the data and stratification of flow to improve the fit of the data to the least variable model. These estimates were then compared to estimates of sediment yield for the proposed construction at each potential site.

Sediment yield for the various training areas was computed using the Revised Universal Soil Loss Equation (RUSLE). This equation uses data derived from local rainfall intensity, frequency, soil types, vegetative cover and conservation practices. The RUSLE equation is given below.

A = R*K*L*S*C*P

Where

A = Annual sediment yield in tons per acre per year

R = Rainfall erosivity factor

K = Soil erodibility factor

L = Length of field (sub-area)

S = Slope of field (sub-area)

C = Crop or canopy cover factor

P = Conservation practice factor

The sediment yield for each training area in the Northern Training Complex was computed for three conditions; existing conditions, conditions during construction, and post-construction conditions. Table 1 lists the values used for each factor in the RUSLE equation for each condition.

The "R" value was determined from Yang (1996, Figure 8.1). The "K" factor was determined based on soil types in the area. The U. S. Department of Agriculture report "Soil Survey of Bullitt and Spencer Counties, Kentucky" was consulted. The predominant soil type in the area for the hillsides is Garmon-Crider, a well-drained loam soil. For the valley areas, the soil type adopted was McGary-Markland, poor to well drained soils with a clayey subsoil. For the Garmon-Grider soils, a value of 0.34 was assigned. For the McGary-Markland soils, a value of 0.29 was assigned. The LS factor was computed based on a formula provided by Yang (1996, Formula 8.2). The cropping or canopy factor used was 0.004 for existing and long-term conditions. This value has been used for established grass meadows as reported in Yang (1996). During construction, the C factor used was 0.70. The conservation practice factor was assumed to be 1.0 for existing and construction conditions. This assumes no contouring. For the long-term condition, this factor was assumed to be 0.80 allowing for some contouring after construction was complete.

The digital terrain elevation data for the Fort Knox area was obtained from the U. S. Geological Survey website for 1:24000 scale map data. The training areas were plotted onto this digital representation of the Fort Knox training areas. Using ARCVIEW, the training areas were superimposed over the digital data grid. This resulted in cells thirty meters on a side comprising the training areas. Using ARCVIEW and the above equations and assigned values, parameters were developed for each cell comprising each training area. The larger areas comprised some 5,500 cells each. The RUSLE equation was then applied to each cell within each training area. Total sediment yield, on an annual basis, was then calculated for each training area for each of the three conditions. Visual analysis of the training area locations and the topographic map allowed the sediment from each area to be assigned to a receiving stream (Table 2).

Results

Discharge data for rivers in the area are presented in Table 3. Although the drainage area for the Salt River at Shepherdsville is about 100 mi² less than that for the Rolling Fork River, discharges are comparable (Figures 2 and 3). Major peak flows occur between December and May but summer and/or fall rain events were observed in 1995, 1996, and 1997 in both rivers. Operation of the dam at Taylorsville Lake on the Salt River provides water management and a less variable flow downstream during rain events. Nearly 40-45% of the flow occurs at a discharge of less than 500 ft³ sec⁻¹ for both rivers and the distribution between ranges for each river is comparable (Figure 4). Other rivers and streams in the study area, although responsive to rain events, provide much lower discharge (e.g., mostly less than 500 ft³ sec⁻¹, Table 3).

Data retrieved from STORET was mostly for infrequent sampling of wells and limited sampling of surface water sites. Most of the data were collected in the period from 1980 to 1982. Maximum and minimum values are reported in Appendix A. Notable high values included concentrations for total phosphorus and dissolved orthophosphorus in an unnamed tributary to Mill Creek, total and dissolved calcium in a spring, total magnesium and sodium in an unnamed tributary to the Salt River, and total aluminum in the water and sediment in the Salt River upstream from Pond Creek and associated with a discharge from a pipe.

General water quality conditions were best described with recently collected data for the Salt River at Shepherdsville and the Rolling Fork River at Boston by the KDEP (Appendix B) and are summarized in Table 4. Similar temperatures were observed at both sites (Figure 5) ranging from near 0 °C in the winter to near 28 °C in the summer. Dissolved oxygen concentrations were also similar between sites and displayed seasonal trends as well (Figure 6). Maximum values, near 12-13 mg L⁻¹ were observed in the winter and lower values, near 5-6 mg L⁻¹ were observed during the summer in August. A concentration near 12 mg L⁻¹ was observed in August indicating that daily primary productivity could result in higher concentrations in the summer. The time of sample collection would influence observations since dissolved oxygen is typically dynamic on a daily cycle with lower concentrations occurring in the early morning and maximum concentrations occurring in the afternoon. Total nonfilterable residue concentrations were mostly below 100 mg L⁻¹ for both sites and increased concentrations were more common for the Rolling Fork River with maximum concentrations exceeding 800 mg L⁻¹ on two occasions coincident with storm events (Figure 7). Dampened or lower concentrations would be expected on the Salt River since the dam at Taylorsville Lake attenuates upstream flows associated with major rainfall events and also likely acts as a trap for sediment deposition. Total organic carbon concentrations ranged mostly from near 2 to near 5 mg L⁻¹ and were generally lower in the Rolling Fork River except for during major runoff events when concentrations approached 10 mg L⁻¹ (Figure 8). Conductivity values ranged from 230 to 550 umhos cm⁻¹ with maximum values occurring in the late summer and in association with major runoff events (Figure 9). Mean conductivity values were near 380 to 400 μmhos ⁻¹. Values were slightly higher in the Salt River most of the period of observation. Total alkalinity concentrations ranged between 50 and 200 mg L⁻¹ as CaCO₃ and, in general, were similar at the two sites (Figure 10). Total Kjeldahl nitrogen concentrations were between 0.2 and 1.0 mg L⁻¹ except for during runoff events in the Rolling Fork River basin and a major runoff event in both basins in 1998 when concentrations approached 2 mg L⁻¹ (Figure 11). Mean values for total Kjeldahl nitrogen were near 0.8 mg L⁻¹. Total phosphorus concentrations were highly variable and ranged from 0.01 to 0.50 mg L⁻¹, with values above 0.35 mg L⁻¹ coincident with major runoff events (Figure 12). Elevated values (e.g., $> 0.20 \text{ mg L}^{-1}$) were observed for both basins but not always coincidentally. Mean values of total phosphorus were near 0.17 mg L⁻¹. Total chloride values ranged between 2 and 40 mg L⁻¹ and were generally slightly higher in the Salt River with a maximum value occurring in 1998 coincident with a major runoff event (Figure 13). Concentrations in the Salt River were generally higher than in the Rolling Fork River. Dissolved sulfate concentrations ranged from 6 to 60 mg L⁻¹ and were similar between sites with the exception of higher concentrations in the Rolling Fork River in June of 1997 and in the Salt River in August of 1997 (Figure 14). Total aluminum concentrations were mostly below 2,000 ug L⁻¹ at both sites with exceptions primarily in the Rolling Fork River 3 times in 1996 and 1 time in 1997 and 1998 when concentrations exceeded 4,000 $\mu g L^{-1}$ and 10,000 $\mu g L^{-1}$ (Figure 15). Total iron concentrations were mostly below 2,000 µg L-1 with values greater than 5,000 ug L⁻¹ occurring primarily in the Rolling Fork River coincident with runoff events (Figure 16). As was observed for total aluminum concentrations, elevated concentrations (e.g., > 20,000 μg L⁻¹ were observed in 1996 and 1998 coincident with major runoff events in the Rolling Fork River basin. Fecal coliform concentrations were mostly low (e.g., < 2,000 counts ml⁻¹) but elevated concentrations were observed in the Salt River coincident with runoff events in 1996 and 1998 (Figure 17).

Heavy metals are also monitored at the KPDES sites and concentration ranges for 1997 to November of 1999 are reported in Table 5. Concentrations were mostly near or below the

detection limit for most constituents and elevated concentrations were not observed for any constituent. Selected outfalls were also monitored for total suspended solids, hardness, pH, oil and grease, and chlorides and results are summarized in Table 6. Concentrations of total suspended solids were below or near the mean value of total nonfilterable residue for the Salt River. In general, reported concentrations were within acceptable limits.

Water quality was sampled in Mill Creek by the Kentucky Department for Environmental Protection (KDEP) at three stations in May of 1982 in Hardin County. Minimum and maximum values for selected constituents are presented in Table 7. In general, conductivity, chloride, and sulfate were high and variable and likely contribute to elevated and variable total dissolved solids. The water could be considered as hard based on alkalinity measurements. Values for pH were near neutral. Nutrient concentrations (nitrogen species and phosphorus) were also elevated and quite variable. Chemical oxygen demand was occasionally high. Suspended solids concentrations were low to moderate and, consequently, the turbidity was relatively low. The study concluded that the major impact to the stream is the discharge of domestic wastewater. which has affected the aquatic life in portions of the stream. Violations of Kentucky Surface Water Standards were observed for free cyanide, undissociated hydrogen sulfide, phthalate esters, unionized ammonia, aluminum, and iron (KDEP 1984). Nutrient levels were greatest at the downstream sites. Low dissolved oxygen (DO) values were observed at the downstream sites and were considered to indicate that diurnal and/or seasonal violations of water quality standards for DO are likely to occur. Sediment data showed only pentachlorophenol above detection limits and arsenic was the only metal with a concentration that could be considered as elevated and indicative of pollution. Biological communities downstream from the Radcliff Wastewater Treatment Plant (WWTP) discharge were drastically reduced in diversity when compared to communities upstream from the WWTP. Upstream communities consisted of typical stream forms while downstream communities were dominated by species tolerant to organic and nutrient enrichment. The stream supports a moderate sport fishery. Recommendations included designation for aquatic life/warmwater aquatic habitat and primary and secondary contact recreation. It was recommended that public use should be avoided due to limited access and potentially dangerous military ordinances.

Results of estimates for loading of total nonfilterable residue using regression analysis provided by FLUX are included in Appendix C and summarized in Table 8. In general, individual regression methods resulted in similar loading estimates between 1 * 10⁸ and 6 * 10⁸ kg year⁻¹ (110,250 and 661,500 tons year⁻¹). Variances were relatively high indicating a need for sampling optimization to better describe concentrations during runoff events. Stratification of the hydrograph for low flow and high flow levels of discharge did not considerably reduce the variance.

Sediment yields for existing, during construction, and long-term conditions for each training area are summarized in Table 9. As would be expected, maximum sediment yield occurs coincident with construction. The highest sediment yield during construction was estimated for Area 12, Cedar Creek range and then by Area 6, the Wilcox site, followed by Area 1 and Area 11, the Yano Range. The number of acres for the Wilcox range seems high. However, the number of acres were determined by draping files provided by Fort Knox personnel over the digital terrain map. Interestingly, the greater acreage at the Wilcox site did not yield the highest sediment load, and was half of the estimate for the Cedar Creek range. This may be attributed to increased removal of material required for the Cedar Creek range and a greater change in topography than exists at the Wilcox site. An analysis of the topography for each range provides the explanation. The Cedar Creek range measures about 1,250 acres. However, 31% of the area in this range has a surface slope of more than 10%. This compares to

15% of the Yano range area and 9% of the Wilcox range having a surface slope of greater than 10%. In addition, the areas with a high slope also have a higher erodibility factor, "K", based on the soil type. Therefore, the higher slope and erodibility increase sediment yield. The yield for Wilcox is high due to the slope being only a little less than that for the Yano range, but the area is 22% larger, as included in this analysis.

Construction of the larger ranges (Yano, Wilcox, Cedar Creek) will result is some filling in the adjacent floodplains. Detailed evaluation, at this stage of the planning, has not been conducted for inclusion in this report. However, some qualitative opinions may be put forth. If floodplain encroachment is of limited length, even if the fill is quite high, then such encroachments do not significantly raise flowlines for high stream flows. When the encroachment is for extended length, even if of modest height, the flowline is likely to be raised considerably. These effects will extend for some distance, depending on the stream slope, width and flow rate, upstream from the encroachment. The result is that flooding will be induced upstream of such encroachments. Detailed construction plans were not analyzed for this study. A cursory evaluation would qualitatively indicate that the Cedar Creek range will not significantly affect Rolling Fork flow lines. However, the tributaries transecting the range may well be affected. Yano Range construction would be expected to have some effect on Rolling Fork flow lines, if the floodplain is raised significantly. Since the Wilcox range is largely already in place, no adverse effects would be expected from improvements to this range on Upper Salt River flowlines.

Potential impacts to water quality include increased runoff of sediments and nutrients, increased temperatures of surface waters, increased runoff of oil and grease associated with increased vehicle traffic. The major period of impact will occur coincident with construction but can be minimized with the use of required best management techniques. There is no conversion factor available to determine the potential increase in suspended solids concentrations associated with increased sediment loading, but concentrations periodically greater than 100 to 200 mg L⁻¹ in the Salt River and Rolling Fork River, respectively, have been observed coincident with runoff events and provide an upper boundary for existing conditions (Figure 7). Increased suspended solids concentrations would likely be confined to the period of construction and continue at lower values while revegetation occurred. Upon complete re-establishment of vegetation, sediment loading to the streams should be near pre-construction levels (Table 9). Areas that drain to the Lower Salt River have a higher potential for adverse impacts associated with sediment loading than areas that drain to the Rolling Fork River since concentrations in the Salt River are typically lower which is considered to be favorable to aquatic life and water quality. While hourly data for temperature was not available to evaluate maximum daily values, temperatures were remarkably consistent between the Salt River and Rolling Fork River, and maximum observed values were between 25 and 28 °C (Figure 5). Instantaneous and timeaveraged (e.g., daily, weekly, monthly, etc.) maximum values would also be expected to increase with a greater solar input if clearing is conducted in close proximity to the streams and lakes. It is difficult to predict the increase in temperature, especially for each site, but increases between 3.3 and 10.5 °C in the average monthly temperature following clear-cutting have been reported (Kochenderfer and Aubertin 1975; Rishel et al. 1982; and Swift, Jr. and Messer 1971). It is likely that the areas that require the most clearing along streams and lakes (e.g., the Wilcox site) will be the most susceptible to increased water temperatures. Increased runoff from oil and grease would likely be the same at each site with differences in actual input to the stream as a function of topography, proximity of roads and parking areas, and implementation of best management practices. Evaluation of KPDES permit data indicate that current practices do not result in excessive concentrations of oil and grease under existing conditions.

The use of buffer zones and maintenance of riparian areas along streams and sinkholes has been recommended and specific guidance has been provided by state agencies. These zones help regulate light and temperature to the streams, provide nutrients to the terrestrial and aquatic community, are a source of woody debris to the streams which impacts velocity and sedimentation patterns, and regulate the flow of water and materials (e.g., nutrients and sediments) for upland areas (Naiman et al. 1993). Implementation of best management practices, such as maintenance of buffer strips, prohibition of skidding over streams, proper road location, and avoidance of logging during prolonged wet periods and replanting of cleared areas during clearing can greatly reduce sediment transport to the nearby streams (Lynch et al. 1985). Castelle et al. (1994) suggest that a buffer zone should have a minimum width of 15 m to be effective at protecting wetlands and streams under most conditions, however a range of 3 to 200 m was found to be most effective with temperature moderation requiring 10-30 m, sediment removal requiring 10-60 m, and nutrient removal requiring 10-100 m. Certainly these widths will vary with site-specific conditions.

Summary

Water quality data recently collected by the KDEP at the Salt River near Shepherdsville, KY and the Rolling Fork River and by Fort Knox personnel on site, as required by the KPDES permit, provide information for describing general water quality conditions of surface waters in the study area. Observed ranges of temperature, dissolved oxygen, and pH are typical for rivers and streams in the area and indicated seasonal patterns that would be expected. Sampling limited to once per day precluded assessment of daily cycles. Concentration ranges for most of the constituents monitored were indicative of hard water surface waters (e.g., high ranges of conductivity, total alkalinity, chloride, sulfate). While total Kjeldahl nitrogen concentrations were generally low (e.g. < 2 mg L⁻¹), total phosphorus values were well above concentrations of 0.02 mg L⁻¹ that are indicative of eutrophic conditions in lakes and reservoirs. However, total organic carbon concentrations near 5 mg L⁻¹ are common in streams and rivers with forested areas in the watershed and are not typically considered to be excessively high concentrations. Concentrations of nonfilterable residue, total iron, and total aluminum were also not typically high, except for during runoff events. Fecal coliform concentrations were generally at acceptable limits for designated uses. Temporal patterns in concentration distributions indicated that elevated concentrations were coincident with selected runoff events and that spatial differences between the 2 sites were minimal except for a few runoff events, which likely occurred differently at each site (e.g., less intense rainfall or localized rainfall at one site). Comparison of recently collected data to data collected in 1982 at Mill Creek suggests that water quality has likely improved since considerably fewer violations are occurring. Loading estimates for total nonfilterable residue indicated that sediment loads in the Salt River at Shepherdsville (near 105,000 to 179,000 tons year⁻¹) were about four times lower than for the Rolling Fork River (near 550,00 to 723,000 tons year⁻¹).

Estimates of sediment yield were highest for the construction period (as would be expected) but accounted for less than 0.2% of the annual load from each training area to the corresponding receiving stream using existing and post-construction conditions (Table 9). During construction, increased sediment accounted for 4 to 8% of the annual load at all sites except for Area 1 (27.5%), Area 6 or the Wilcox site (40.1%), and Area 12 or the Cedar Creek range (21.5%). The extremely high yields during construction are deceiving. These are based on no conservation practices during construction such as the erection of sediment barriers, hay bale

dams and construction of temporary berms to prevent sediment from leaving the construction site. The construction specifications will undoubtedly call for such measures. Also, these figures are based on annual yield. Again, the actual construction period may be only a few months in length, or the site may be constructed in phases so that smaller areas are disturbed at any one time. Barring a catastrophic failure, the actual sediment loss from the site should be much less with conservation practices in place during construction. An increase over the existing sediment yield may be on the order of 150-200%.

Estimates of annual sediment yields during construction could account for a considerable part of the total annual sediment load to the Rolling Fork and Salt River, however, implementation of best management practices, adjustment of annual sediment yields to a projected length of construction, and construction during periods of minimum rainfall would greatly reduce the sediment load associated with runoff. Using the increase in the percent of the annual sediment load indicates that construction at the Wilcox site will have the most measurable impact on water quality followed by Area 1 and the Cedar Creek range.

Recommendations to provide considerable reductions in potential adverse impacts on water quality associated with construction and utilization of the completed project include maintenance of buffer zones and implementation of best management practices during construction. Construction should be scheduled, if possible, to avoid periods when rainfall events normally occur to minimize transport of material from the watershed to the streams and rivers with runoff.

Table 1. Values used in the Revised Universal Soil Loss Equation.

Factor	Existing	Construction Period	Post-construction
R	195	195	195
K	(0.34 for hill areas,	(0.34 for hill areas,	(0.34 for hill areas,
	0.29 for valley areas)	0.29 for valley areas)	0.29 for valley areas)
LS	Computed for each	Computed for each	Computed for each
	sub area	sub area	sub area
С	0.004	0.70	0.004
P	1.0	1.0	0.80

Table 2. Training areas and associated receiving streams.

Training Area	Receiving Stream
1	Lower Salt River
2	Lower Salt River
3	Lower Salt River
4	Lower Salt River
5	Lower Salt River
6	Upper Salt River
9	Upper/Lower Salt River
10	Lower Salt River
11	Rolling Fork River
12	Cedar Creek/Rolling Fork River

Table 3. Summary of available discharge data for the Fort Knox area.

River or Stream	USGS Station ID	Drainage Area (miles ²)	Comments
		()	(average or range of flow)
Salt River at	03298500	1197	Retrieved 1990-1999
Shepherdsville, KY			$(1700 \text{ ft}^3 \text{ sec}^{-1})$
Rolling Fork at	03301500	1299	Retrieved 1995-1999
Boston, KY			$(1800 \text{ ft}^3 \text{ sec}^{-1})$
Rolling Fork Near	03299000	239	1990-1992 only
Lebanon, KY			$(2000-5000 \text{ft}^3 \text{sec}^{-1})$
Mill Creek Near Fort	03301700	38.2	1999 only
Knox, KY			(<200 ft ³ sec ⁻¹)
Plum Creek Near	03296500	19.1	1955-1961
Wilsonville, KY			$(<700 \text{ ft}^3 \text{ sec}^{-1})$
Wilson Creek Near	03301580	27.7	1991-1996
Deatsville, KY			$(<200 \text{ ft}^3 \text{ sec}^{-1})$
Long Lick at	03298550	7.91	1992-1999
Clermont, KY			$(<200 \text{ ft}^3 \text{ sec}^{-1})$
Elm Lick Near	03298535	0.68	1975-1985 Peak Flow
Clermont, KY			only $(50-800 \text{ ft}^3 \text{ sec}^{-1})$
			,
Brier Creek at	03302050	n/a	1999
Pendelton Road			$(10-40 \text{ ft}^3 \text{ sec}^{-1})$

Table 4. Summary statistics for the KDEP water quality data (1995-1998).

Salt River															
	WATER	WATER CNDUCTVY	8	표	T ALK (CHLORIDE SULFATE RESIDUE	SULFATE		TORGC	TOT HARD	TOT HARD NH3+NH4- NO2&NO3	NO2&NO3	TOT KJ	PHOS-T	TOT KJIPHOS-T(FEC COLI
	TEMP	FIELD		-	CACO3 TOTAL		S04-DISS	TOT NFLT C		CACO3	N TOTAL	N-TOTAL	z	_	MFM-FCBR
	CENT	MICROMHO MG/L		SU	MG/L	MG/L	MG/L	MG/L	MG/L I	MG/L	MG/L	MG/L	MG/L	MG/LP	/100ML
													- 1		
Mean	13.5636	404.727273		9.009 7.648	142.68	11.857143	28.07429	50.08571	4.131429	50.08571 4.131429 177.45714	0.0576	0.0576 1.0117143	0.6658 0.16477	0.16477	1867.5
Std. Dev.	7.58769	62.1310474	2.595 0.245	0.245	29.626	7.0841283	13.74286	69,45772 1.303789		44.284072	44.284072 0.0219628 0.4462292	0.4462292	0.311	0.311 0.09537	3573.40827
	1.32085	10.8156271	0.459 0.044	0.044	5.0808	1.1974362	2.322967	11.7405	11.7405 0.220381	7.4853743	7.4853743 0.0037124 0.0754265	0.0754265	1	0.01612	0.0526 0.01612 893.352068
	0.4	265	4.7	7	49	3	10	1	2.2	11	0.05	0.11	0.159	0.018	10
	27.7	554	13.1	8.1	188	41	58.6	382	6.6	235	0.166	2.02	1.8	0.431	12000
	33	33	32	31	34	35	35	35	35	35	32	35	35	35	16
Rolling Fork															
Near															
Lebanon														1	1
Junction	10	94	300	400	410	940	946	530	680	006	610	630		999	31616
	WATER	WATER CNDUCTVY DO	8	H	T ALK	CHLORIDE SULFATE RESIDUE	SULFATE		T ORG C	TOT HARD	T ORG C TOT HARD NH3+NH4- NO2&NO3	NO2&NO3		PHOS-T	TOT KUIPHOS-T(FEC COLI
-	TEMP	FIELD			CACO3 TOTAL		S04-DISS	S04-DISS TOT NFLT C		CACO3	N TOTAL	N-TOTAL	z		MFM-FCBR
	CENT	MICROMHO MG/L	MG/L	SU	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L P	/100ML
Mean	13.7581	379.032258		8.855 7.597	142.12	7.2571429	32.79429		218.4 3.817647		185.11429 0.0598286	0.798	0.7645	0.7645 0.15751	384
Std. Dev.	7.58524	62.3685198		2.332 0.194	30.42	4.3679505	14.02808		643.1444 1.850712		0.0287172	34.70868 0.0287172 0.4870367		0.4707 0.14041	470.33119
Std. Err.	1.36235	11.2017168	l	0.419 0.036	5.217	0.7383184	2.371178		108.7112 0.317394	5.8668376		0.0048541 0.0823242	0.0796	0.0796 0.02373	121.438991
	1.4	236	5.5	7.1	72	2	9	1	1.3	104	0.05	0.05	0.175	0.01	30
	26.6	510	13.3	8	202	23	61.2	3800	6.6	255	0.201	1.94	1.99	0.534	1400
	31	31	31	29	34	32	35	32	34	35	35	35	35	35	15

Table 4. Summary statistics for the KDEP water quality data (1995-1998).

Salt River														
	ALUMINUM ARSENIC CADMIUM CH	ARSENIC	CADMIUM	CHROMIUM	ROMIUM COPPER IRON		LEAD	MANGNESE MERCURY ZINC	MERCURY		CALCIUM	CALCIUM MGNSIUM PTSSIUM SODIUM	PTSSIUM	SODIUM
	AL,TOT	AS,TOT	ср,тот	CR,TOT	CU,TOT	FE,TOT PB,TOT	PB,TOT	MN	HG,TOTAL	5	CA-TOT	MG,TOT	КТОТ	NA.TOT
	UG/L			UG/L	UG/L	UG/L	UG/L	UG/L	UG/L	UG/L	MG/L	MG/L		MG/L
Mean	986.4	2.028571	-	1.82857143	1.942857	1534.5	2.42857	1534.5 2.42857 200.1142857	0.0742857	6.0286	56.01143	10.348571	3.196857	6.94543
Std. Dev.	912.027709 0.169031	0.169031	0	1.38236188	1.714006	1373.1	1.03713	1.03713 460.9711469	0.0253546	6.2095		10.62073 2.5129513	0.906596	3,3684
Std. Err.	154.16082	0.028571	0	0.23366181	0.28972	232.09	0.17531	232.09 0.17531 77.91834523	0.0042857	1.0496		1.795231 0.4247663	0.153243	0.56936
Min	102	2	1	1	1	209	2	27	0.05	2	19	5.5		2.73
Max	4280	က	1	9	6	6270	7	2810	0.1	36	71.7	14.8		17.3
E	35	35	35	35	35	35	35	35	35	35	35	35	35	35
Rolling Fork														
Near							•							
Lebanon														
Junction	1105	1002	1027	1034	1042	1045	1051	1055	71900	1092	916	927	937	929
	Σ	ARSENIC	CADMIUM	CHROMIUM	ROMIUM COPPER	IRON	LEAD	MANGNESE	MERCURY ZINC		CALCIUM	CALCIUM MGNSIUM	PTSSIUM	SODIUM
	٥ م	Ь	<u>о</u>	CR,TOT	CU,TOT	FE,TOT	PB,TOT	NW	HG, TOTAL ZN, TOT CA-TOT	ZN,TOT		MG,TOT	K,TOT	NA,TOT
	UG/L	UG/L	UG/L	UG/L	NG/L	NG/L	UG/L	UG/L	UG/L	UG/L	MG/L	MG/L	MG/L	MG/L
Mean	2071.17143	2.2	-	2.57142857	2.971429	3990.3	3990.3 3.57143	166.7428571	0.0728571	11.286	54.15143	12.12	2.958571	4.95457
Std. Dev.	2657.14744 0.719477	0.719477	0	2.17317488	2.628864	5248.1	5248.1 2.95342	137.662277	0.0252716	13.073	9.724662	2.9570255	0.762516	2.79939
Std. Err.	449.139892 0.121614	0.121614	0	0.3673336	.3673336 0.444359	887.09	0.49922	887.09 0.49922 23.26917183	0.0042717	2.2098	1.643768	0.4998285	0.128889	0.47318
Min	191	2	-	-	1	604	2	44	0.05	2	31.9	5.9	1	1.37
Max	10800	9		80	13	22300	17	299	0.1	22	73.2	18.1	4.19	15.2
u	35	35	32	32	35	32	32	35	35	35	35	35	35	32

Table 5. Concentration ranges for selected heavy metals and mercury at the KPDES monitoring

sites for the Fort Knox facility (1997-1999).

Constituent (mg L ⁻¹)	Minimum	Maximum
T. Cadmium	BDL	0.0006
T. Chromium	0.001	0.036
T. Copper	BDL	0.018
T. Lead	0.002	0.072
T. Mercury	0.0001	0.0009
T. Silver	BDL	0.002
T. Nickel	0.003	0.027
T. Zinc	0.001	0.049
PH (standard units)	7.4	8.8

Table 6. Reported discharge and proposed limits for selected water quality constituents at

selected outfalls on Fort Knox (1997 Permit).

Constituent	Reported	Reported	Proposed	Proposed
	Discharge	Discharge	Limits	Limits
	Monthly	Daily	Monthly	Daily
	Average	Maximum	Average	Maximum
Outfall 003				
Flow (MGD) *	27.2	42	Report	Report
Total Suspended Solids (mg L ⁻¹)	11.4	36	Report	Report
Hardness (as mg L ⁻¹ CaCO ₃)	210	225	Report	Report
pH (standard units)	7.9 (min)	8.0	Report	Report
Outfall 004				
Flow (MGD)	30.4	43	Report	Report
Total Suspended Solids (mg L ⁻¹)	12.3	47	Report	Report
Hardness (as mg L ⁻¹ CaCO ₃)	206	215	Report	Report
pH (standard units)	7.9 (min)	8.0	Report	Report
Outfall 005				
Flow (MGD)	38	58	Report	Report
Total Suspended Solids (mg L ⁻¹)	12.8	56	Report	Report
Hardness (as mg L ⁻¹ CaCO ₃)	203	210	Report	Report
pH (standard units)	7.9 (min)	8.0	Report	Report
Outfall 006				
Flow (MGD)	47.8	65	Report	Report
Total Suspended Solids (mg L ⁻¹)	12.3	50	Report	Report
Hardness (as mg L ⁻¹ CaCO ₃)	203	210	Report	Report
pH (standard units)	7.9 (min)	8.1	Report	Report
Outfall 017				
Discharge Flow (MGD)	0.0005	0.0005	Report	Report
Salt River Flow (MGD)	1,544	2,921	Report	Report
Total Suspended Solids (mg L ⁻¹)	92.3	387	30	60
Oil and Grease (mg L ⁻¹)	3.2	4.0	10	15
pH (standard units)	7.3 (min)	7.7	6.0 (min)	9.0
Discharge Chlorides (mg L ⁻¹)	39,522	42,000	Report	Report

^{*} MGD = million gallons per day

Table 7. Range of selected chemical constituent concentrations from Mill Creek, KY (1982).

Constituent	Minimum	Maximum
Conductivity (µmhos cm ⁻¹)	429	1043
pH (standard units)	7.0	7.8
Dissolved Oxygen (mg L ⁻¹)	4.0	7.6
BOD ₅ (mg L ⁻¹)	1.4	7.7
COD (mg L ⁻¹)	2.9	37.0
Alkalinity (mg L ⁻¹)	152.0	159.2
Chloride (mg L ⁻¹)	12.3	143.2
Turbidity (NTUs)	6.2	6.5
Total Dissolved Solids (mg L ⁻¹)	262	600
Suspended Solids (mg L ⁻¹)	4.0	38.0
Sulfate (mg L ⁻¹)	51.9	102.4
NH ₃ -N (mg L ⁻¹)	0.13	7.34
$NO_2 + NO_3 - N \text{ (mg L}^{-1})$	0.345	4.4
TKN (mg L ⁻¹)	0.59	7.64
Total Phosphorus (mg L ⁻¹)	0.05	8.4
Dissolved Orthophosphorus (mg L ⁻¹)	0.006	7.8
Total Aluminum (µg L ⁻¹)	292	1250
Dissolved Aluminum (µg L ⁻¹)	131	292
Total Iron (μg L ⁻¹)	190	1156
Dissolved Iron (µg L ⁻¹)	15	52

Table 8. Estimated loading of total nonfilterable residue for Salt River and Rolling Fork River.

	Salt River	Rolling Fork
Average Flow (ft ³ sec ⁻¹)	1711	1840
FLUX	$* 1.626 \times 10^8$	* 6.556 x 10 ⁸
(Flow Weighted Avg Conc)		
(*Kg year ⁻¹) (** tons year ⁻¹)	** 179,266.5	** 722,799
Estimated Load	* 0.960 x 10 ⁸	* 4.999 x 10 ⁸
(Avg Conc * Avg Flow)		
(*Kg year ⁻¹) (** tons year ⁻¹)	** 105,840	** 551,139.8

Table 9. Annual sediment yield for the training sites for existing, construction, and post-construction conditions.

	-	Existina		Construction		Long term		
Training Area	Designation	(tons/yr)	% load		% load	% load (tons/year)	% load	Acres*
Area1		225	0.158	39360	27.611	180	0.126	541
Area2		43	0.030	7575	5.313	35	0.024	108
Area3		73	0.051	12843	9.009	29	0.041	220
Area4		64	0.045	11198	7.856	51	0.036	131
Area5		35	0.024	8609	4.236	28	0.019	81
Area6	Wilcox	328	0.230	57467	40.312	328	0.230	1509
Area9		63	0.044	11060	7.759	51	0.035	93
Area10		37	0.026	9629	4.487	29	0.021	265
Area11	Yano	220	0.035	38499	6.044	176	0.028	1234
Area12	Cedar Crk	784	0.123	137160	21.533	627	0.098	1225
Notes								
*	* As computed for sediment yield calculations	for sediment	yield calc	ulations				
*	Annual yield,	should be adi	usted bas	** Annual yield, should be adjusted based on projected length of construction	d length c	of construction	uc	

NORTHERN TRAINING COMPLEX

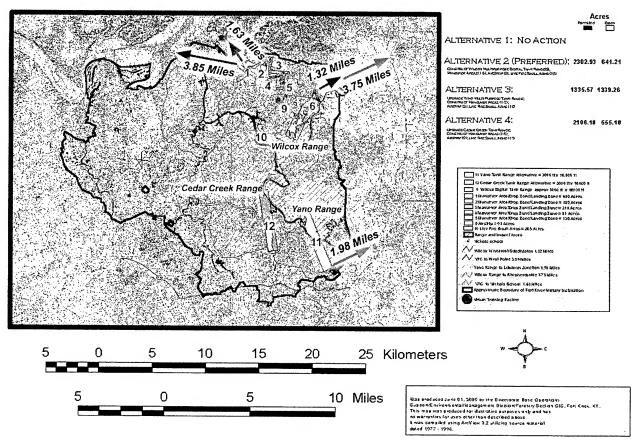


Figure 1. Proposed training sites for the Northern Training Complex.

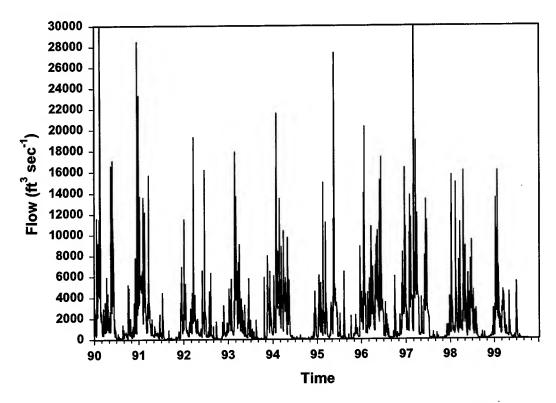


Figure 2. Discharge for the Salt River at Shepherdsville, KY, 1990-1999.

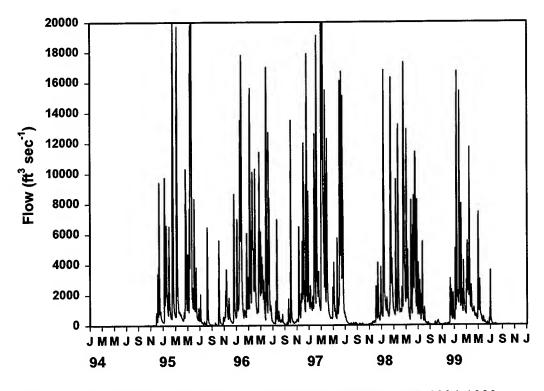


Figure 3. Discharge for the Rolling Fork River at Boston, KY, 1994-1999.

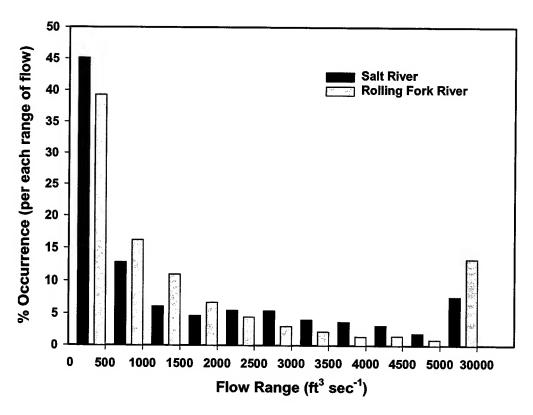


Figure 4. Frequency distribution of flow ranges for the Salt River and Rolling Fork River.

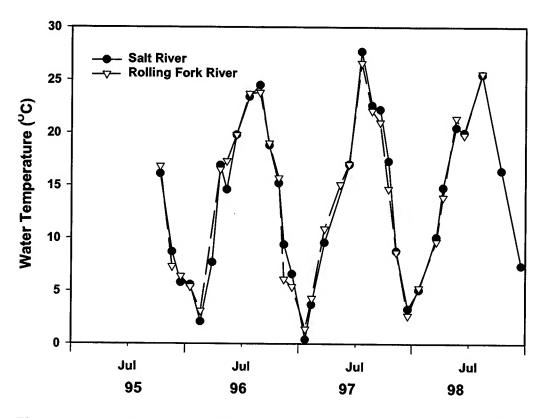


Figure 5. Temperature values for the Salt River and Rolling Fork River, 1995-1998.

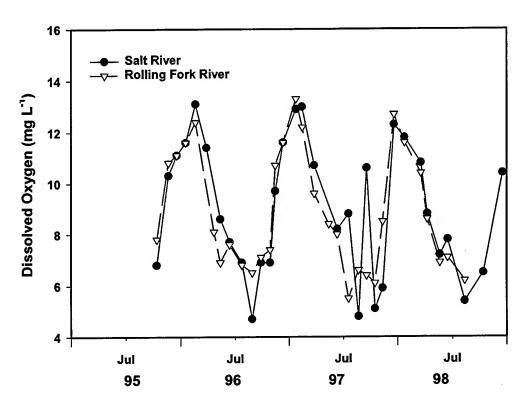


Figure 6. Dissolved oxygen concentrations for the Salt River and Rolling Fork River, 1995-1998.

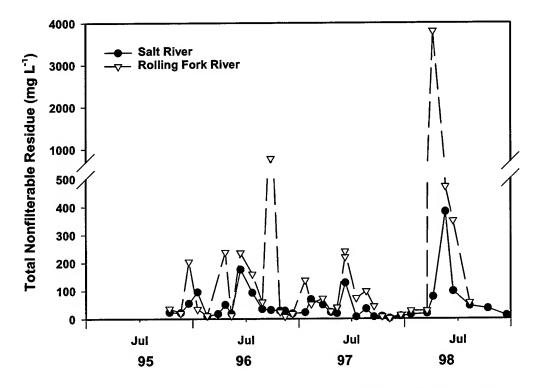


Figure 7. Total nonfilterable residue concentrations for the Salt River and Rolling Fork River, 1995-1998.

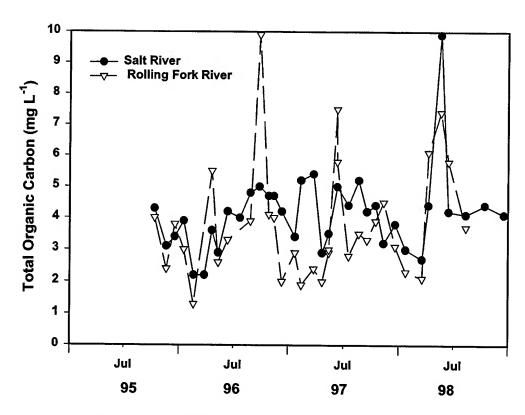


Figure 8. Total organic carbon concentrations for the Salt River and Rolling Fork River, 1995-1998.

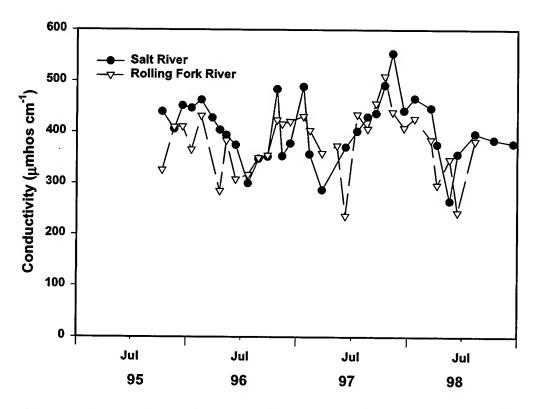


Figure 9. Conductivity values for the Salt River and Rolling Fork River, 1995-1998.

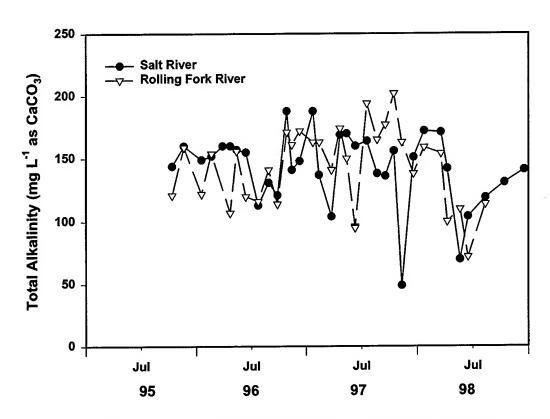


Figure 10. Total alkalinity values for the Salt River and Rolling Fork River, 1995-1998.

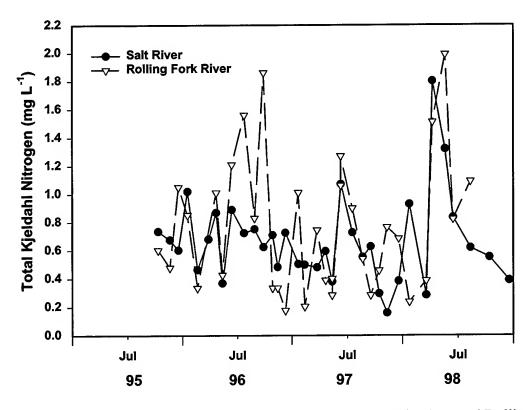


Figure 11. Total Kjeldahl nitrogen concentrations for the Salt River and Rolling Fork River, 1995-1998.

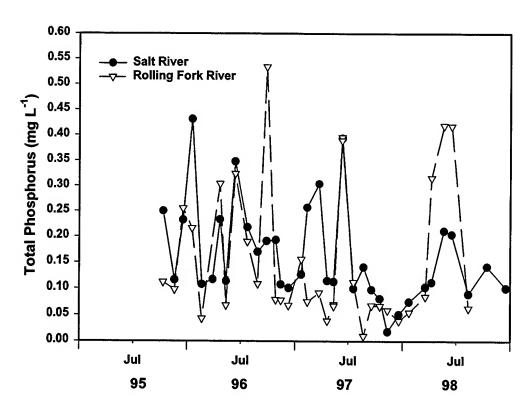


Figure 12. Total phosphorus concentrations for the Salt River and Rolling Fork River, 1995-1998.

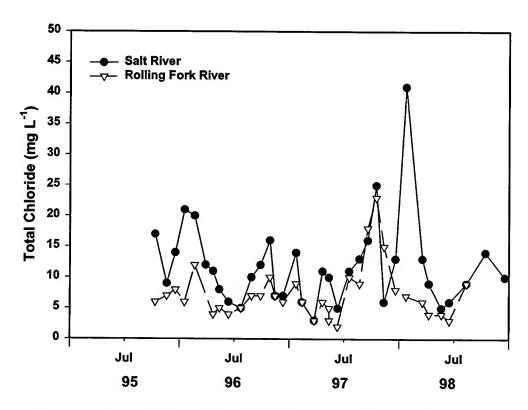


Figure 13. Total chloride concentrations for the Salt River and Rolling Fork River, 1995-1998.

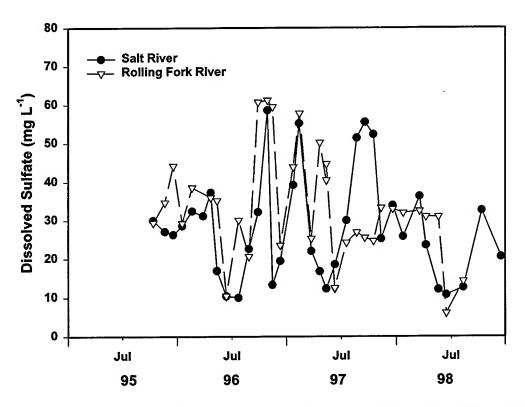


Figure 14. Dissolved sulfate concentrations for the Salt River and Rolling Fork River, 1995-1998.

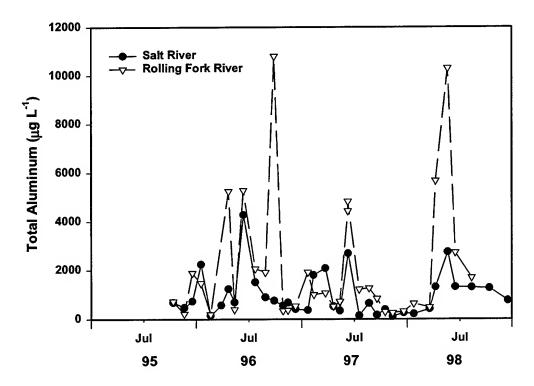


Figure 15. Total aluminum concentrations for the Salt River and Rolling Fork River, 1995-1998.

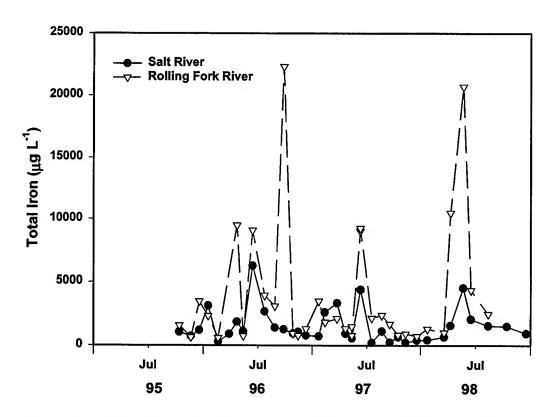


Figure 16. Total iron concentrations for the Salt River and Rolling Fork River, 1995-1998.

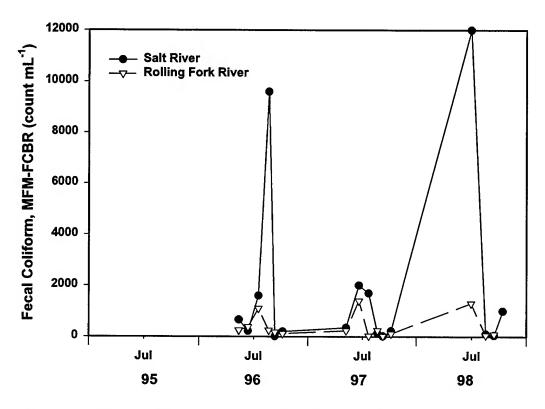


Figure 17. Fecal coliform counts for the Salt River and Rolling Fork River, 1995-1998.

References

Castelle, A.J., Johnson, A.W., and Conolly, C. 1994. Wetland and stream buffer size requirements – A review, J. Environ. Qual., 23:878-882).

Kentucky Department for Environmental Protection. 1984. Mill Creek Drainage Biological and Water Quality Investigation, Technical Report No. 12, Kentucky Department of Environmental Protection Division of Water, Frankfort, KY.

Kentucky Department for Environmental Protection. 1998. Kentucky Watershed Framework – Status Report of the Salt River Watershed, Kentucky Department of Environmental Protection Division of Water, Frankfort, KY.

Kentucky Division of Water. 1998. State of the River, A report on the condition of the Salt River watershed, Kentucky, and the minor Ohio River tributaries in the area, November 1998, Kentucky Department of Environmental Protection Division of Water, Frankfort, KY.

Kochenderfer, J.N. and Aubertin, G.M. 1975. Effects of management practices o water quality and quantity – Fernow Experimental Forest, West Virginia, In Proc., Municipal Watershed Management Symposium, Gen. Tech. Rep. NE-13. For. Serv., U.S. Dept., Agr., Broomall, Penn. pp.14-24.

Lynch, J.A., Corbell, E.S., and Mussallem, K. 1985. Best management practices for controlling nonpoint-source pollution on forested watersheds, J. Soil and Water Cons., 40:164-167.

Naiman, R.J., Décamps, H. and Pollock, M. 1993. The role of riparian corridors in maintaining regional biodiversity, Ecol. Appl., 3(2):209-212.

Payne, B.S. and Green, W. 2001. Biological assessment of streams associated with the Northern Training Complex at Ft. Knox, KY, August, 2000, Letter Report, Environmental Laboratory, Waterways Experiment Station, U.S. Army Engineer Research and Development Center, Vicksburg, MS.

Rishel, G.B., Lynch, J.A., and Corbett, E.S. 1982. Seasonal stream temperature changes following forest harvesting, J. Environ. Qual., 11(1):112-116.

Swift, L.W., Jr., and Messer, J.B. 1971. Forest cuttings raise temperatures of small streams in the southern Appalachians, J. Soil and Water Cons., 26(3):111-115.

Walker, W.W. 1996. Simplified procedures for eutrophication assessment and prediction: User's Manual, Instruction Report W-96-2, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Yang, C.T. 1996. Sediment Transport, Theory and Practice. McGraw-Hill, New York, NY, 393 pp.

Appendix A Minimum and Maximum Values for Selected Water Quality Constituents in the STORET Database

PARAMETER	DESCRIPTION	MAXIMUM	MINIMUM
	Water Temp Cent	29.5	11.5
11	Water Temp Faren	85.8	52.7
	TURB (FTU)	15	2.1
	TRANSP Secchi (in)	42	24
	CNDUCTVY Field (umho)	450	430
95	CNDUCTVY @25 C (umhos)	1860	245
299	DO mg/l	7	6
	DO % sat	92.1	76.9
310	BOD5 mg/l	7	1.4
335	COD mg/l	37	2.9
340	COD mg/l	28	28
400	PH su	7.9	6.6
403	PH su	7.8	6.8
410	T Alk mg/l CaCO3	252	152
	RESIDUE (TNFR) mg/l	38	102
	OIL-GRSE mg/l	1	1
	DISS. Nitrogen mg/l	1.5	3
	ORG nitrogen mg/l	0.17	0.17
	NH3+NH4- Nit, Diss mg/l	0.03	0.03
	NH3+NH4- Nit, Total mg/l	7.3	0.03
	UN-IONZD NH3-N mg/l	1.00E-04	0.00003
	NO2-N, Diss. mg/l	0.07	0.0003
	NO3-N, Diss. mg/l	1.2	1.2
	UN-IONZD NH3-N mg/l	2.00E-04	0.00003
	NO3-N. Total mg/l	1.25	1.25
	KJELDL Nit., Diss. mg/l	0.2	0.1
	TOT Kjeldahl Nit mg/l	7.64	0.5
	NO2&NO3 Nit, Total mg/l	4.4	0.35
	NO2&NO3, Nit, Diss. mg/l	14	0.02
	PHOS-TOT, mgP/l	8.4	0.05
	PHOS-DIS mgP/I	0.05	0.03
	PHOS-DIS. Ortho, mgP/I	7.8	0.006
	Total Organic Carbon mg/l	7.6	0.2
	CYANIDE, Total mg/l	0.005	0.003
	CYANIDE, Free mg/l	0.04	0.04
	SULFIDE, Diss. mg/l	0.1	0.1
	Total Hardness CaCO3 mg/l	340	140
	NC Hardness mg/l	89	1
	CALCIUM, Diss mg/l	110	48
	CALCIUM. Total mg/l	91	44
	MGNSIUM, Diss mg/l	19	3.4
	MGNSIUM, Total mg/l	19.1	10.5
	SODIUM, Total mg/l	65	8.75
	SODIUM, Diss mg/l	16	2.7
	PTSSIUM, Diss mg/l	1.7	1
	PTSSIUM, Total mg/l	10.1	2
	CHLORIDE, Total mg/l	290	3
	SULFATE, Total mg/l	1000	1

PARAMETER	DESCRIPTION	MAXIMUM	MINIMUM
950	FLUORIDE, Diss mg/l	0.9	0.1
955	SILICA, Diss mg/l	13	9
1002	ARSENIC, Total mg/l	50	2
1005	BARIUM, diss ug/l	42	41
	BARIUM, total ug/l	95	46
1010	BERYLIUM, diss ug/l	1	1
1012	BERYLIUM, total ug/l	10	10
	CADMIUM, diss ug/l	3	1
	CADMIUM, total ug/l	10	3
	CHROMIUM, diss ug/l	10	1
1034	CHROMIUM, total ug/l	2	1
1035	COBALT, diss ug/l	3	3
	COBALT, total ug/l	20	20
	COPPER, ug/l	10	3
1042	COPPER, total ug/l	16	10
1044	IRON, susp ug/l	1100	70
1045	IRON, total ug/l	1156	80
1046	IRON, diss ug/l	62	4
	LEAD, diss ug/l	15	10
1051	LEAD, total ug/l	25	18
1054	MANGNESE, susp ug/l	70	0
1055	MANGNESE, total ug/l	220	10
1056	MANGNESE, diss ug/l	182	0
1059	THALLIUM, total ug/l	100	100
1060	MOLY, diss ug/l	10	10
1062	MOLY, total ug/l	20	20
1064	TELLURUM, total ug/l	40	40
1067	NICKEL, total ug/l	23	8
1077	SILVER, total ug/l	10	
	STRONTUM, diss ug/l	81	58
1082	STRONTUM, total ug/l	310	160
1085	VANADIUM, diss ug/l	6	6
· 1087	VANADIUM, total ug/l	10	
1090	ZINC, diss ug/l	170	
	ZINC, total ug/l	100	
1097	ANTIMONY, total ug/l	40	
1102	TIN, total ug/l	100	
	ALUMINUM, total ug/l	2400	
	ALUMINUM, diss ug/l	353	
1108	AL, MUD Dry Wt mg/kg-Al	28300	
1147	SELENIUM, total ug/l	50	
1153	TITANIUM, total ug/l	102	102

Appendix B Data from the Kentucky Division of Water Monitoring Program

LOCATION	DATE	Jday	TIME	DEPTH	10	94	3	300	400	-	410	
					WATER	CNDUCTVY	8		PH	 -	TALK	
					TEMP	FIELD				S	CACO3	
					CENT	MICROMHO	MG/L	7	SU	Σ	MG/L	
SAL I RIVER AT SHEPHERDSVILLE	951012		1120	1	16.1	440	®	6.8	7.6	(G)	144	(6)
SALI RIVER AI SHEPHERDSVILLE	951120	324	1135	0.983999	8.7 @	406	9	10.3 @	7.8	(e)	160	(8)
SALT RIVER AT SHEPHERDSVILLE	951218	352	1115	0.983999	@ 8·S	452	6)	11.1	7.9	(e)		(e
SALT RIVER AT SHEPHERDSVILLE	960117	382	1055	0.983999	5.6	447	 	-) (G	149	9
SALT RIVER AT SHEPHERDSVILLE	960219	415	1240	0.983999	2.1	463	<u> </u>	13.1) @		0
SALT RIVER AT SHEPHERDSVILLE	960328	452	1125	0.983999	-	428	ـــــ		7.9	9 @		0
SALT RIVER AT SHEPHERDSVILLE	960422	477	1110	0.983999	16.9	404	1) (e	160) (6
SALT RIVER AT SHEPHERDSVILLE	960513	498	1200	0.983999	14.6	394	_	8.6	7.4) (6) (6
SALT RIVER AT SHEPHERDSVILLE	960613	529	1130	0.983999	19.8	375	\perp		7.6) (e	+	0
SALT RIVER AT SHEPHERDSVILLE	960718	564	1205	0.983999	0		6	(G)) (G		0
SALT RIVER AT SHEPHERDSVILLE	960724	570	1110	0.983999	23.4 @	300	6.	6	7.5) (G)	113) (e
SALI RIVER AT SHEPHERDSVILLE	960822	299	1110	0.983999	0		(G)	6		(e)		(e
SALT RIVER AT SHEPHERDSVILLE	960828	605	1120	0.983999	24.5 @	348		4.7 @	7.5) @	131	9 (
SALT RIVER AT SHEPHERDSVILLE	960912	620	1120	0.983999	(0)		_) @) (0
SALT RIVER AT SHEPHERDSVILLE	960927	635	1200	0.983999	18.8	352		6.9	7.7) (G	121	0
SALT RIVER AT SHEPHERDSVILLE	961008	646	1220	0.983999	(B)		(8)	@	_) (G)	_) (e
SALT RIVER AT SHEPHERDSVILLE	961028	999	1055	0.983999	15.2 @	484	_	6.9	7.5	9 (8)	188	0
SALT RIVER AT SHEPHERDSVILLE	961114	683	1510	0.983999	9.4	353 @		9.7 @	7.3) (e)		(e
SALT RIVER AT SHEPHERDSVILLE	961210	209	1100	0.983999	9.9	378 @	11.6		7.6	0	+	(a)
SALI RIVER AI SHEPHERDSVILLE	970122	752	198	0.983999	_		12.9	@	7.6	(9)	188	(9)
SALT RIVER AT SHEPHERDSVILLE	970212	772	930	0.983999		357 @		13 @	7.5	(9)	137 ((9)
SALI RIVER AI SHEPHERDSVILLE	970324	813	1240	0.983999	9.6	287 @	10.7	9		(a)	104	@
SALI RIVER AI SHEPHERDSVILLE	970421	841	1145	0.983999	(a)	0	0	(9)		(0)	169 ((0)
SALT BIVER AT SHEPHERDSVILLE	970508	828	1115	0.983999	(9)	(9)	(3)	0	9	@		(0)
OALT RIVER AT SHEPHERDSVILLE	970513	863	1030	0.983999			0)	(9)	9	@	170	(9)
OALT RIVER AT SHEPHERDSVILLE	970610	892	400	0.983999	17 @	371 @		8.2 @	9.7	(a)	160	(9)
SALI RIVER AL SHEPHERDSVILLE	970620		1215	0.983999	0	©	0	(9)	9	ම		9
SALI KIVEK AI SHEPHERDSVILLE	970719		1140	0.983999	27.7	402 @	80	@ @	8	@	164	6
SALI RIVER AI SHEPHERDSVILLE	970723	934	1115	0.983999	@	(3)	0	(9)		(a)		(e)
SALI RIVER AI SHEPHERDSVILLE	970822	964	915	0.983999	22.6	430 @		4.8	7.5	(8)	138	(e)
SAL I RIVER AT SHEPHERDSVILLE	970822		1600	0.983999	@			(9)		(a)		(e)
SALI RIVER AI SHEPHERDSVILLE	970909	_	1045	0.983999	0	0	_	(9)	9	(e)	9	(G)
SALT RIVER AT SHEPHERDSVILLE	970918	- 1	1135	0.983999	22.2 @	437	10.6	6@	8.1	(a)	136	(0)
SALT BIVER AT SHEPHERDSVILLE	971007	- 1	1115	0.983999	(8)			$\overline{}$		(9)		(9)
SALI KIVER AI SHEPHERUSVILLE	971016	1019	88	0.983999	17.3 @	492 @	5.1	9	7.3 @	9	156 ((0)

NATER CNDUCTVY DO	LOCATION	DATE .	Jdav	TIME	DEPTH	9	-	94	-	300	4	400	410	0	
TEMP FIELD MCRONHO MCRIL SUME SU						WATER	O	NDUCTVY	Ω	0	표		T ALK		
TOTALITY						TEMP	됴	ELD					CACO3	_	
971111 1045 1210 0.983999 8.8 6 554 6 5.9 7 940129 1118 1445 1021 0.983999 3.3 442 6 11.3 0 11.3 0 11.3 0 11.3 0 11.3 0 11.3 0 11.3 0 11.3 0 11.3 0						CENT	Σ	ICROMHO	Σ	G/L	SU		MG/L		
971219 1083 925 0.983999 3.3 442 12.3 6 7.9 <th< td=""><td>SALT RIVER AT SHEPHERDSVILLE</td><td>971111</td><td>1045</td><td>1210</td><td>0.983999</td><td></td><td>3</td><td>-</td><td>(A)</td><td>6</td><td>(G)</td><td>7 @</td><td></td><td>49 @</td><td></td></th<>	SALT RIVER AT SHEPHERDSVILLE	971111	1045	1210	0.983999		3	-	(A)	6	(G)	7 @		49 @	
980123 1118 1145 0.983999 5.1 @ 466 @ 11.8 @ 7.9 [980219 1173 900 0.983999 10.1 @ 347 @ 10.8 @ 7.8 [980221 1226 825 0.983999 20.6 @ 265 @ 7.2 @ 7.4 [980221 1226 825 0.983999 20.6 @ 357 @ 7.8 @ 7.5 [980221 1226 825 0.983999 20.6 @ 357 @ 7.8 @ 7.5 [980212 1215 0.983999 20.6 @ 357 @ 7.8 @ 7.5 [980212 1319 0.983999 2.6 @ 37 @ 265 @ 7.5 [980212 1319 0.983999 2.6 @ 37 @ 265 @ 7.5 [980212 1319 0.983999 16.4 @ 385 @ 6.5 @ 7.7 [980212 1319 0.983999 16.4 @ 385 @ 6.5 @ 7.7 [980212 1319 0.983999 16.4 @ 385 @ 6.5 @ 7.7 [980212 1319 0.983999 17.3 @ 326 @ 7.7 [980212 1320 0.983999 17.3 @ 326 @ 7.7 [980212 1319 0.983999 17.3 @ 326 @ 7.7 [980212 1319 0.983999 17.3 @ 326 @ 7.7 [980212 1310 0.983999 17.3 @ 326 @ 7.7 [980213 324 1210 0.983999 17.3 @ 326 @ 7.7 [980214 1322 1200 0.983999 17.3 @ 326 @ 7.7 [980215 324 1210 0.983999 17.3 @ 326 @ 7.7 [980217 322 1200 0.983999 17.3 @ 326 @ 11.6 @ 7.7 [980218 324 1210 0.983999 17.3 @ 326 @ 7.4 [980219 415 1330 0.983999 17.3 @ 326 @ 7.4 [980219 415 1330 0.983999 13.5 @ 326 @ 7.4 [980219 415 1330 0.983999 13.5 @ 326 @ 7.4 [980219 415 1330 0.983399 13.5 @ 326 @ 7.4 [980219 415 1330 0.983399 13.5 @ 326 @ 7.4 [980219 415 1330 0.983399 13.5 @ 326 @ 6.5 @ 7.7 [980219 415 1330 0.983399 13.5 @ 326 @ 7.4 [980219 415 0.983399 13.8 @ 326 @ 7.4 [980219 415 0.983399 13.8 @ 326 @ 7.4 [980210 4110 0.983399 13.8 @ 326 @ 6.5 @ 7.7 [980210 426 1313 0.983399 15.7 @ 424 @ 7.4 [980210 4110 0.983399 13.8 @ 424 @ 7.4 [980210 4110 0.983399 13.8 @ 424 @ 7.4 [980210 4110 0.983399 13.8 [980210 4114 683 1610 0.983399 14.4 @ 431 @ 13.3 [980210 4112 0.983399 15.2 @ 421 [980210 4113 0.983399 15.4 @ 424 [980210 4113 0.983399 15.2 @ 424 [980210 4113 0.983399 15.4 @ 424 [980210 4113 0.983399 15.4 @ 424 [980210 4113 0.983399 15.4 @ 424 [980210 4113 0.983399 15.4 [980210 4114 683 1610 0.983399 14.4 [980210 4114 683 1610 0.983399 14.4 [980210 4114 683 1610 0.983399 14.4 [980210 4114 683 1610 0.983399 14.3 [980210 442 0.983399 14.4 [980210 442 0.083399 14.4 [980210 442 0.083399	SALT RIVER AT SHEPHERDSVILLE	971219	1083	925	0.983999		(9)		(3)		(B)	(9)			
980319 1173 900 0.983999 10.1 447 0 10.8 9 8 0 10.983999 10.1 447 0 10.8 9 8 0 10.83999 10.1 0 376 0 10.8 0 7.8 0 0 7.8 0 7.8	SALT RIVER AT SHEPHERDSVILLE	980123	1118	1145	0.983999		(3)		(S)		(6)	_		<u>8</u>	
980409 1194 925 0.983999 14.8 @ 376 @ 8.8 Ø 7.8 980616 12.36 825 0.983999 20.5 @ 265 Ø 7.2 Ø 7.4 Ø 7.5 Ø	SALT RIVER AT SHEPHERDSVILLE	980319	1173	006	0.983999		(3)		(S)		(B)	_	171	9	0)
980E21 1236 825 0.983999 20.5 @ 265 @ 7.2 @	SALT RIVER AT SHEPHERDSVILLE	980409	1194	925	0.983999		(a)	376	3				142	2	
980616 1262 840 0.983999 20 357 7.8 7.5 980617 1276 1330 0.983999 26.5 397 6 7.8 7.6 980818 1325 1215 0.983999 16.4 6 6 6 7.6 980818 1325 1215 0.983999 16.4 6 6 6 7.6 981014 1382 1205 0.983999 16.4 6 6 7.7 INCTION 981014 1382 1205 0.983999 16.4 6 7.8 7.7 INCTION 961012 286 0.983999 16.8 326 7.8 7.7 INCTION 961012 285 0.983999 16.8 326 11.1 6 7.7 INCTION 960112 252 1200 0.983999 16.5 6 6 6 7.7 INCTION 960513 415 330 0.983999	SALT RIVER AT SHEPHERDSVILLE	980521	1236	825	0.983999	20.5	(9)	265	(8)					20	0)
980630 1276 1330 0.983999 25.5 99 96 54 7.6 980812 1319 900 0.983999 25.5 99 397 6 54 7.6 980818 1325 1215 0.983999 6 6 6 6 6 7.6 980816 1382 1300 0.983999 16.4 385 6 6.5 7.7 981014 1382 1200 0.983999 16.4 378 10.4 7.7 JNCTION 951217 1446 1110 0.983999 16.8 6 7.8 7.7 JNCTION 960219 324 1210 0.983999 16.8 6 7.8 7.7 JNCTION 960422 477 1230 0.983999 16.5 6 7.8 7.7 JNCTION 960513 498 1310 0.983999 16.5 6 6 6 7.8 JNCTION 9605	SALT RIVER AT SHEPHERDSVILLE	980616	1262	840	0.983999		(8)		(3)	œ			104	4	(A)
980812 1319 900 0.983999 25.5 90 397 6 5.4 7.6 980818 1325 1215 0.983999 6 6 6 6 7.7 980816 1325 1215 0.983999 16.4 6 6 6 7.7 980915 1352 1205 0.983999 16.4 6 6 6 7.7 981014 1382 1205 0.983999 7.4 6 7.8 7.7 JNCTION 95120 2.983999 7.3 410 0 10.8 7.7 JNCTION 951218 352 1200 0.983999 7.3 411 0 11.6 7.7 JNCTION 960213 451 130 0.983999 15.6 386 6.5 7.8 7.7 JNCTION 960422 477 1220 0.983999 15.2 0 386 0 1.6 7.7 JNCTION	SALT RIVER AT SHEPHERDSVILLE	980630	1276	1330	0.983999		(6)	9	(3))	©	<u>@</u>		0	0)
980818 1325 1215 0.983999 ©	SALT RIVER AT SHEPHERDSVILLE	980812	1319	006	0.983999	2	(a)		3	4		_	119	<u>@</u> 6	(A)
980915 1353 1300 0.983999 16.4 0 98 0	SALT RIVER AT SHEPHERDSVILLE	980818	1325	1215	0.983999		(e)	9	(3)	9	(a)	@		0	(A)
981014 1382 920 0.983999 16.4 0 385 0 6.5 0 7.7 MCTION 981014 1382 1205 0.983999 7.4 0 378 0 0.0 0 7.8 0 7.7 MCTION 951120 2.983999 7.4 0 378 0 10.4 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 7.8 0 0 7.8 0 7.8 0 7.8 0 0 7.8 0 0 7.8 0 7.8 0 0 0 7.8 0 0 0 7.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0	SALT RIVER AT SHEPHERDSVILLE	980915	1353	1300	0.983999		(e)	9	(S)		(a)	0		0	(2)
981014 1382 1205 0.983999 7.4 0 378 0 0 7.7 TION 951012 285 0.983999 7.4 0 378 0 10.4 0 7.7 TION 951012 285 0.983999 7.3 0 10.983999 7.3 0 10.4 0 7.8 0 7.7 TION 951120 3.24 1210 0.983999 6.4 0 411 0 7.8 <t< td=""><td>SALT RIVER AT SHEPHERDSVILLE</td><td>981014</td><td>1382</td><td>920</td><td>0.983999</td><td></td><td>(9)</td><td></td><td>(3)</td><td>2</td><td></td><td>-</td><td>131</td><td>1 @</td><td>(2)</td></t<>	SALT RIVER AT SHEPHERDSVILLE	981014	1382	920	0.983999		(9)		(3)	2		-	131	1 @	(2)
100 Mode 378 (matrix) 1446 1110 0.983999 7.4 (matrix) 378 (matrix) 10.4 (matrix) 7.8 (matrix)	SALT RIVER AT SHEPHERDSVILLE	981014	1382	1205	0.983999		(9)	9	(S)		@	<u>@</u>		0	(A)
TION 9551012 285 0.983999 16.8 © 326 © 7.8 © 7.8 7.	SALT RIVER AT SHEPHERDSVILLE	981217	1446		0.983999	7.4	(9)		ල) (න				141	10	0)
TION 951120 324 1210 0.983999 7.3 410 0 10.8 0 7.8 TION 9601218 352 1200 0.983999 6.4 411 0 11.1 0 7.9 TION 960219 415 1330 0.983999 16.5 0 285 0 11.6 0 7.9 TION 960219 415 1330 0.983999 16.5 0 285 0 8.1 0 7.9 TION 960213 430 0.983999 17.3 0 384 0 6.9 7.7 TION 960613 529 1220 0.983999 19.8 0 7.6 0 7.7 TION 960718 564 1720 0.983999 23.7 0 6.8 0 7.6 0 7.7 TION 960822 590 1045 0.983999 23.7 0 6.8 0 0	ROLLING FORK NEAR LEBANON JUNCTION	951012	285		0.983999		(G)	326	ල)	7.8			121	<u>7</u>	(C)
TION 951218 352 1200 0.983999 6.4 @ 411 @ 11.1 @ 7.9 110N 960117 382 1155 0.983999 3.1 @ 432 @ 11.6 @ 8 110N 960219 415 1330 0.983999 16.5 @ 285 @ 8.1 @ 7.7 120N 960613 429 1230 0.983999 17.3 @ 384 @ 6.9 @ 7.3 170N 960613 529 1230 0.983999 17.3 @ 308 @ 7.6 @ 7.6 170N 960622 599 1045 0.983999 19.8 @ 317 @ 6.8 @ 7.4 170N 960822 599 1045 0.983999 23.7 @ 317 @ 6.8 @ 7.4 170N 960822 599 1045 0.983999 23.8 @ 350 @ 6.5 @ 7.7 170N 960822 599 1045 0.983999 19 @ 350 @ 6.5 @ 7.7 170N 960822 620 1050 0.983999 19 @ 355 @ 7.1 @ 7.7 170N 960922 620 1050 0.983999 19 @ 355 @ 7.1 @ 7.7 170N 960922 635 1305 0.983999 15.7 @ 424 @ 7.4 @ 7.5 170N 961028 666 1130 0.983999 15.7 @ 424 @ 10.7 @ 7.8 170N 961028 666 1130 0.983999 15.7 @ 421 @ 10.7 @ 7.8 170N 961028 666 1130 0.983999 6.1 @ 421 @ 10.7 @ 7.8 170N 96121 752 1215 0.983999 1.4 @ 421 @ 1.6 @ 7.6 7.6 7.6 7.8	ROLLING FORK NEAR LEBANON JUNCTION	951120	324	1210	0.983999	7.3	(9)		ම	10.8		7.8 @	159	@ 6	(a)
TION 960117 382 1155 0.983999 5.4 9 366 0 11.6 8 TION 960219 415 1330 0.983999 3.1 432 0 12.4 0 7.7 TION 960422 477 1230 0.983999 16.5 0 285 8.1 0 7.6 TION 960613 529 1230 0.983999 19.8 0 7.6 0 7.7 TION 960718 564 1120 0.983999 23.7 0 317 0 6.8 0 7.7 TION 960822 599 1045 0.983999 23.7 0 317 0 6.8 0 7.7 TION 960822 599 1045 0.983999 23.8 0 6.8 0 7.7 0 TION 960822 599 1045 0.983999 23.8 0 6.8 0 7.4	ROLLING FORK NEAR LEBANON JUNCTION	951218	352	1200	0.983999	6.4	(9)		<u>@</u>			7.9 @		<u>@</u>	(a)
TION 960219 415 1330 0.983999 3.1 @ 432 @ 12.4 @ 7.7 TION 960422 477 1230 0.983999 16.5 @ 285 @ 8.1 @ 7.6 TION 960513 498 1310 0.983999 17.3 @ 8.4 @ 6.9 7.6 TION 960613 529 1230 0.983999 19.8 @ 7.6 0 7.6 TION 960724 570 1220 0.983999 23.7 @ 6.8 0 7.7 TION 960828 605 1220 0.983999 23.8 @ 55.0 0 7.7 TION 960827 620 1050 0.983999 19.6 0.983999 19.6 6.5 0 7.1 0 7.1 0 7.1 0 7.1 0 7.1 0 7.1 0 7.1 0	ROLLING FORK NEAR LEBANON JUNCTION	960117	382	1155	0.983999	5.4	(9)		(9)		@		122	2 @	(S)
TION 960422 477 1230 0.983999 16.5 © 285 © 8.1 © 7.6 TION 960513 498 1310 0.983999 17.3 © 384 © 6.9 7.6 TION 960613 529 1230 0.983999 19.8 © 308 © 7.6 0 7.7 TION 960724 570 1220 0.983999 23.7 © 9 7.4 © 7.7 TION 960822 599 1045 0.983999 23.8 © 6.5 © 7.7 TION 960828 605 1220 0.983999 19 © 6.5 Ø 7.7 TION 960912 620 1050 0.983999 15.7 © 424 Ø 7.4 Ø 7.4 Ø 7.7 TION 961028 666 1130 0.983999 15.7 Ø 421	ROLLING FORK NEAR LEBANON JUNCTION	960219	415	1330	0.983999	3.1	(9)		(9)					<u>4</u>	(a)
TION 960513 498 17.3 @ 384 @ 6.9 7.3 TION 960613 529 1230 0.983999 19.8 @ 7.6 0 7.6 TION 960718 564 1120 0.983999 23.7 @ 0 0 0 7.6 0 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.6 7.7 1.2 0.983999 23.7 0 0 0 0 0 7.7 0 0.983999 23.8 0 0 0 0 7.7 0 0.983999 19 0	ROLLING FORK NEAR LEBANON JUNCTION	960422	477	1230	0.983999	16.5	(9)		(e)					00/2	(9)
TION 960613 529 1230 0.983999 19.8 @ 308 @ 7.6 7.6 7.6 7.6 TION 960718 564 1120 0.983999 23.7 @ 6.8 @ 7.4 TION 960822 599 1045 0.983999 23.8 @ 6.8 @ 7.7 TION 960822 699 1045 0.983999 23.8 @ 6.5 @ 7.7 TION 960927 635 1305 0.983999 19 @ 6.5 @ 7.7 TION 961028 666 1130 0.983999 15.7 @ 424 @ 7.4 @ 7.8 TION 961028 666 1130 0.983999 6.1 @ 424 @ 7.4 @ 7.8 TION 961028 666 1133 0.983999 6.1 @ 424 @ 7.4 @	ROLLING FORK NEAR LEBANON JUNCTION	960513	498		0.983999	17.3	(6)		(9)		_			156@	(a)
TION 960718 564 1120 0.983999 23.7 0 0 0 0 7.4 TION 960822 599 1045 0.983999 23.7 0 0 0 0 7.4 TION 960822 599 1045 0.983999 23.8 0 6.5 0 7.7 TION 960828 605 1220 0.983999 23.8 0 6.5 0 7.7 TION 960927 635 1305 0.983999 19 0 355 0 7.4 0 7.5 TION 961028 666 1130 0.983999 15.7 0 424 7.4 7.5 TION 961028 666 1133 0.983999 6.1 0 0 0 0 0 TION 961028 666 1130 0.983999 6.1 0 424 0 7.4 0 7.8 TION <td>ROLLING FORK NEAR LEBANON JUNCTION</td> <td>960613</td> <td>529</td> <td></td> <td>666286'0</td> <td>19.8</td> <td>(9)</td> <td>308</td> <td>(9)</td> <td></td> <td></td> <td></td> <td></td> <td>120 @</td> <td>(S)</td>	ROLLING FORK NEAR LEBANON JUNCTION	960613	529		666286'0	19.8	(9)	308	(9)					120 @	(S)
TION 960724 570 1220 0.983999 23.7 @ 6.8 7.4 TION 960822 599 1045 0.983999 23.8 @ 6.5 @ 7.7 TION 960828 605 1220 0.983999 23.8 @ 6.5 @ 7.7 TION 960927 635 1305 0.983999 19 @ 6.5 @ 7.7 TION 961028 666 1130 0.983999 15.7 @ 424 @ 7.4 @ 7.5 TION 961028 666 1130 0.983999 15.7 @ 424 @ 7.4 @ 7.5 TION 961028 666 1130 0.983999 6.1 @ 424 @ 7.4 @ 7.8 TION 961028 666 1130 0.983999 6.1 @ 424 @ 7.4 @ 7.8 <t< td=""><td>ROLLING FORK NEAR LEBANON JUNCTION</td><td>960718</td><td>564</td><td></td><td></td><td></td><td>(a)</td><td>-</td><td>(9)</td><td></td><td></td><td></td><td></td><td>0</td><td>(A)</td></t<>	ROLLING FORK NEAR LEBANON JUNCTION	960718	564				(a)	-	(9)					0	(A)
TION 960822 599 1045 0.983999 23.8 @ 65 @ @ % TION 960828 605 1220 0.983999 23.8 @ 65 % 7.7 TION 960912 620 1050 0.983999 19 @ 65 % 7.1 @ 7.7 TION 961008 646 1150 0.983999 15.7 @ 424 @ 7.4 @ 7.5 TION 961028 666 1133 0.983999 15.7 @ 424 @ 7.4 @ 7.5 TION 961028 666 1133 0.983999 6.1 @ 416 @ 7.6 7.5 TION 961028 666 1133 0.983999 6.1 @ 416 @ 7.6 7.6 TION 961210 7.983999 6.1 @ 421 @ 11.6 7.6 7.6<	ROLLING FORK NEAR LEBANON JUNCTION	960724	570		0.983999	23.7	(9)		(9)					116@	(8)
TION 960828 605 1220 0.983999 23.8 @ 350 @ 6.5 @ 7.7 TION 960912 620 1050 0.983999 19 @ 60 0 7.1 0 7.7 TION 960927 635 1305 0.983999 19 @ 60 7.1 0 7.7 TION 961028 666 1130 0.983999 15.7 @ 424 0 7.4 0 7.5 TION 961028 666 1133 0.983999 6.1 0 416 0 7.6 7.8 TION 961028 666 1133 0.983999 6.1 0 416 0 10.7 0 7.8 TION 961210 709 1130 0.983999 6.1 0 421 0 11.6 0 7.6 TION 961210 752 1215 0.983999 6.1	ROLLING FORK NEAR LEBANON JUNCTION	960822	299				a	-	(9)		_		0)	(0)	(A)
TION 960912 620 1050 0.983999 19 0 355 0 7.1 0 TION 960927 635 1305 0.983999 19 0 355 0 7.1 0 7.7 TION 961028 666 1130 0.983999 15.7 0 424 0 7.4 0 7.5 TION 961028 666 1133 0.983999 6.1 0 424 0 7.4 0 7.5 TION 961028 666 1133 0.983999 6.1 0 416 0 10.7 0 7.8 TION 961210 709 1130 0.983999 6.1 0 421 0 10.7 0 7.6 TION 961210 709 1130 0.983999 1.4 0 431 0 13.3 0 7.6 TION 970212 773 1025 0.983999 4.	ROLLING FORK NEAR LEBANON JUNCTION	960828	605		0.983999	23.8	(9)	_	(9)				141	_	ക
TION 960927 635 1305 0.983999 19 © 355 © 7.1 © 7.1 TION 961008 646 1150 0.983999 15.7 © 424 © 7.4 © 7.5 TION 961028 666 1133 0.983999 6.1 © 424 © 7.4 © 7.5 TION 961028 666 1133 0.983999 6.1 © 416 © 10.7 © 7.8 TION 961210 709 1130 0.983999 6.1 © 421 © 7.8 TION 961210 709 1130 0.983999 5.4 © 421 © 7.6 TION 970122 752 1215 0.983999 4.3 @ 431 © 13.3 © 7.6 TION 970212 773 1025 0.983999 4.3 @ 404	ROLLING FORK NEAR LEBANON JUNCTION	960912	620				(a)		(9)	_	(B)	Ø	<u></u>	<u>(a)</u>	(8)
TION 961008 646 1150 0.983999 15.7 0 424 0 7.4 0 7.5 TION 961028 666 1133 0.983999 6.1 0 424 7.4 7.4 7.5 TION 961028 666 1133 0.983999 6.1 0 416 0 7.8 TION 961210 709 1130 0.983999 6.1 0 421 0 11.6 7.6 TION 970122 752 1215 0.983999 1.4 0 431 0 13.3 0 7.6 TION 970212 773 1025 0.983999 4.3 0 404 0 12.2 0 7.6	ROLLING FORK NEAR LEBANON JUNCTION	960927	635			19	(9)		(9)	_				114 @	(A)
TION 961028 666 1130 0.983999 15.7 @ 424 @ 7.4 @ 7.5 TION 961028 666 1133 0.983999 6.1 @ 416 @ 10.7 @ 7.8 TION 961210 709 1130 0.983999 6.1 @ 421 @ 11.6 @ 7.6 TION 970122 752 1215 0.983999 1.4 @ 431 @ 13.3 @ 7.6 TION 970212 773 1025 0.983999 4.3 @ 404 @ 12.2 @ 7.6		961008	646				(9)		(9)		(B)	Ø	0)	0	(9)
TION 961028 666 1133 0.983999 6.1 0 416 0 0 7.8 TION 961214 683 1610 0.983999 6.1 0 4416 0 10.7 7.8 TION 961210 709 1130 0.983999 5.4 0 421 11.6 0 7.6 TION 970122 773 1025 0.983999 4.3 0 404 0 12.2 0 7.6		961028	999			15.7	(a)		(9)				0	0	(A)
TION 961114 683 1610 0.983999 6.1 @ 416 @ 10.7 @ 7.8 TION 961210 709 1130 0.983999 5.4 @ 421 @ 11.6 @ 7.6 TION 970122 752 1215 0.983999 1.4 @ 431 @ 13.3 @ 7.6 TION 970212 773 1025 0.983999 4.3 @ 404 @ 12.2 @ 7.6	ROLLING FORK NEAR LEBANON JUNCTION	961028	999				9	<u> </u>	(9)		(a)	Ø		171 @	(6)
TION 961210 709 1130 0.983999 5.4 @ 421 @ 11.6 @ 7.6 (TION 970122 752 1215 0.983999 4.3 @ 404 @ 12.2 @ 7.6 (TION 970212 773 1025 0.983999 4.3 @ 404 @ 12.2 @ 7.6		961114	683			6.1	@		(9)	10.7		7.8 @		161	ക
TION 970122 752 1215 0.983999 1.4 @ 431 @ 13.3 @ 7.6 (10.0) 970212 773 1025 0.983999 4.3 @ 4.3 @ 704 @ 12.2 @ 7.6	ROLLING FORK NEAR LEBANON JUNCTION	961210	709			5.4	(0)	$\overline{}$	(9)			7.6		172 @	(A)
TION 970212 773 1025 0.983999 4.3 @ 404 @ 12.2 @ 7.6	ROLLING FORK NEAR LEBANON JUNCTION	970122	752	_		1.4	©	-	(9)						ക
	ROLLING FORK NEAR LEBANON JUNCTION	970212	773			4.3	<u></u>	_	(e)	7	_			163	(9)

LOCATION	DATE	Jday	TIME	DEPTH	10	94	4	300		400	410	0
					WATER	CNDUCTVY	ļ	8	풉	_	TALK	
	-				TEMP	FIELD					CAC03	ဗ
					CENT	MICROMHO		MG/L	SU	_	MG/L	
ROLLING FORK NEAR LEBANON JUNCTION	970324	813	1145	0.983999	10.9	359	@	9.6	a	(0)	141	@
ROLLING FORK NEAR LEBANON JUNCTION	970421	841	1255	0.983999	9	@	@		(9)	(0)		174 @
ROLLING FORK NEAR LEBANON JUNCTION	970508	828	1100	0.983999	9	0	(9)		(9)	(0)	0	(9)
ROLLING FORK NEAR LEBANON JUNCTION	970513	863	1150	0.983999	15.1	374	@	8.4	(9)	7.8	Ĺ	150 @
ROLLING FORK NEAR LEBANON JUNCTION	970513	863	1155	0.983999)	@	(9)		(9)	(0)		150@
ROLLING FORK NEAR LEBANON JUNCTION	970610	891	1205	0.983999	17 (@ 236	@	8	(a)	7.5 @		@ 96
ROLLING FORK NEAR LEBANON JUNCTION	970610	891	1210	0.983999	0	(a)	(9)		(0)	0		
ROLLING FORK NEAR LEBANON JUNCTION	970620	901	1305	0.983999	0	©	(9)		(a)	(8)		©
ROLLING FORK NEAR LEBANON JUNCTION	970719	930	1310	0.983999	26.6	9 435	@	5.5	(9)	7.6 @	194	
ROLLING FORK NEAR LEBANON JUNCTION	970723	934	1045	0.983999	0	@	(9)		(9)	(0)	0	(9)
ROLLING FORK NEAR LEBANON JUNCTION	970822	964	1010	0.983999	22.1 @	9 407	(0)	9.9	(0)	7.7	165	6
ROLLING FORK NEAR LEBANON JUNCTION	970822	964	1515	0.983999	@	(2)	(9)		(a)	(8)	0)	(3)
ROLLING FORK NEAR LEBANON JUNCTION	970909	982	1005	0.983999	0	8)	8		(a)	(8)		(8)
ROLLING FORK NEAR LEBANON JUNCTION	970918	991	1215	0.983999	21 @	9 457	(9)	6.4	(a)	7.4 @	1777	_
ROLLING FORK NEAR LEBANON JUNCTION	971007	1010	1100	0.983999	@	0)	(9)		(9)	(0)		(9)
ROLLING FORK NEAR LEBANON JUNCTION	971016	1019	1240	0.983999	14.7 @	510	0	6.1	(a)	7.3 @	202	8
ROLLING FORK NEAR LEBANON JUNCTION	971111	1045	1300	0.983999	8.7 @	9 440	@	8.5	(a)	7.1	163	3
ROLLING FORK NEAR LEBANON JUNCTION	971219	1083	1100	0.983999	(a)	0	@		(9)	0	138	8
ROLLING FORK NEAR LEBANON JUNCTION	971219	1083	1200	0.983999	2.7 @	409	@	12.7	(a)	@		(9)
ROLLING FORK NEAR LEBANON JUNCTION	971219	1083		0.983999	(a)		(9)		(a)	@	138	8
ROLLING FORK NEAR LEBANON JUNCTION	980123	1118	1245	0.983999			(9)	11.6	(9)	7.8 @		@
ROLLING FORK NEAR LEBANON JUNCTION	980319	1173	90	0.983999	\rightarrow		0		(a)	7.7 @	154	@
ROLLING FORK NEAR LEBANON JUNCTION	980409	1194	1020	0.983999			(0)	$\overline{}$	(a)	7.5 @	100	0
ROLLING FORK NEAR LEBANON JUNCTION	980521	1236	915	0.983999			(9)		(B)	7.5 @	110	@
ROLLING FORK NEAR LEBANON JUNCTION	980616	1262	930	0.983999	19.8	243	(0)	7.1	0	7.4 @		72 @
ROLLING FORK NEAR LEBANON JUNCTION	980630	1276	1300	0.983999	0	0)	(9))	@	@		(9)
ROLLING FORK NEAR LEBANON JUNCTION	980812	1319	1030	0.983999	25.6 @	383	(9)	6.2	@	0.7	114	4
	980818	1325	1145	0.983999	(a)	0	(6))	@	@		(9)
_ 11	980915	1353	1230	0.983999	(B)		(9)		(B)	0		@
	981014	1382	1020	0.983999	15.2 @	373	(9)	7.8	(3)	7.7 @	142	2@
	981014	1382	1140	0.983999	®		(9)	9	(B)	@		(9)
ROLLING FORK NEAR LEBANON JUNCTION	981217	1446	1200	0.983999	5.6@	381	0	11.1	@	7.8 @	134	6

SALT RIVER AT SHEPHERDSVILLE	RIDE	L + 4 L		000	000	-	2	_	1	770	_
		SOLTAIL		RESIDUE	T ORG C	ALU	ALUMINUM	AF	ARSENIC	CADMIUM	
	_	S04-DISS		TOT NFLT	ပ	AL,TOT	ОТ	AS	AS,TOT	ср,тот	
SALT RIVER AT SHEPHERDSVILLE		MG/L	_	MG/L	MG/L	NG/L	•	NG/L	3/L	UG/L	
SALT RIVER AT SHEPHERDSVILLE	17 @	30	(9)	23 @	4.3	@	929	©	2 K	_	ᅩ
SALT RIVER AT SHEPHERDSVILLE	@	27.1	(9)		3.1 (@		@	2 K	1	1 K
SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE	14 @	26.3	(9)	54 @	3.4	0	728 (@	2 K		1 K
SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE	21 @		0	95 @	3.9	@	2240 @	(9)	2 @		ᅩ
SALT RIVER AT SHEPHERDSVILLE	20 @		(0)	@ 6	2.2	(9)	147 ((9)	2 K		1 K
SAI T RIVER AT SHEPHERDSVII I F	12 @	31.2 @	9	17 @	2.2	@	999	0	2 K		۲ ۲
	11 @		(9)	50 @	3.6	(a)	1230	(a)	2 K		1 K
SALT RIVER AT SHEPHERDSVILLE	8	16.9	(9)		2.9	®	989	(9)	2 K	1	ᅩ
SALT RIVER AT SHEPHERDSVILLE	9	10.4	(9)	176 @	4.2	@	4280	(9)	2 K	1	ᅩ
SALT RIVER AT SHEPHERDSVILLE	0	8	(9)	8		®		ම	®	-	0
SALT RIVER AT SHEPHERDSVILLE	5	10	(9)	93 @	4	(a)	1510 (@	2 K	_	노
SALT RIVER AT SHEPHERDSVILLE	9		(9)	8		(a)		(a)	(8)		0
SALT RIVER AT SHEPHERDSVILLE	10 @	22.6	(9)	8 (9)	4.8	(a)	891 ((B)	2 K		쏘
SALT RIVER AT SHEPHERDSVILLE	9	©	(9)	®		@)	@	@		0
SALT RIVER AT SHEPHERDSVILLE	12 (32.2	(0)	31 @	2	(a)	751	@	2 K	•	쏘
SALT RIVER AT SHEPHERDSVILLE	9	0	(0)	8		ම		(0)	©	-	0
SALT RIVER AT SHEPHERDSVILLE	16 (@ 58.6	(9)	28 @	4.7	@	551 (@	2 K	_	1 X
SALT RIVER AT SHEPHERDSVILLE	7 (13.3	(9)	28 @	4.7	©	673	(a)	2 K		7
SALT RIVER AT SHEPHERDSVILLE	7		(9)		4.2	@	404	@	2 K		ㅈ
SALT RIVER AT SHEPHERDSVILLE	14 (39.2	(9)	22 @	3.4	(a)	362	@	2 K		1 X
SALT RIVER AT SHEPHERDSVILLE	9	@ 55.2	9	@ 69	5.2	@	1800	(a)	2 K		7
SALT RIVER AT SHEPHERDSVILLE	3(22	(9)	20 @	5.4	0	2080	©	2 K		ㅈ
SALT RIVER AT SHEPHERDSVILLE	11	16.7	(9)	23 @	2.9	@	217	(9)	2 K		ᅩ
SALT RIVER AT SHEPHERDSVILLE	9	@	@	0		@		(0)	(9)	0	0
SALT RIVER AT SHEPHERDSVILLE	10 (0 12.3	(0)	18 @	3.5	(B)		®	2 X	`	ㅗ
SALT RIVER AT SHEPHERDSVILLE	5 (18.5		128 @	5	(B)	2690	(a)	2 X	`	ㅗ
SALT RIVER AT SHEPHERDSVILLE	9	@	0	<u>@</u>		(a)		(a)	0	0	®
SALT RIVER AT SHEPHERDSVILLE	11 (30 a	9	9	4.4	@	135	(9)	3		ㅗ
SALT RIVER AT SHEPHERDSVILLE		@	(9)	0		@		@	<u>@</u>	0	(9)
SALT RIVER AT SHEPHERDSVILLE	13 (@ 51.4	@	35 @	5.5	@	641	®	2 K		논
SALT RIVER AT SHEPHERDSVILLE)	@	(9)	0		(B)		(a)	8	0	0
SALT RIVER AT SHEPHERDSVILLE	9	9	@	0		(a)		(a)	0)	0	<u>@</u>
SALT RIVER AT SHEPHERDSVILLE	16 (@ 55.5	®	9	4.2	ම	161	(a)	2 7		ㅈ
SALT RIVER AT SHEPHERDSVILLE)	@	0	0	0)	ම		®	©	0	0
SALT RIVER AT SHEPHERDSVILLE	25 (2 52.3		8	4.4	@	388	@	2 K		두

LOCATION	940	946	530	089	1105	1002	1027
	CHLORIDE	SULFATE	RESIDUE	T ORG C	ALUMINUM	ARSENIC	CADMIUM
	TOTAL	S04-DISS	TOT NFLT	U	AL,TOT	AS,TOT	CD,TOT
	MG/L	MG/L	MG/L	MG/L	UG/L	NG/L	UG/L
SALT RIVER AT SHEPHERDSVILLE	@ 9			3.2 @	102 @		<u>-</u> ح
SALT RIVER AT SHEPHERDSVILLE	13 @		00 6	3.8	251 @		-
SALT RIVER AT SHEPHERDSVILLE	41 @		14 @	3@	207 @		<u>-</u> ح
SALT RIVER AT SHEPHERDSVILLE	13 @	36.3 @	18@	2.7 @	408		<u>-</u>
SALT RIVER AT SHEPHERDSVILLE	0 6	23.5 @	78	4.4	1300		<u>۔</u> ج
SALT RIVER AT SHEPHERDSVILLE	5 @	12.1 @	382	@ 6.6	2740		<u>-</u>
SALT RIVER AT SHEPHERDSVILLE	9	10.7	86	4.2 @	1300		<u>-</u> ح
SALT RIVER AT SHEPHERDSVILLE	®	0	(a)	®		(9)	(8)
SALT RIVER AT SHEPHERDSVILLE	0 6	12.6	46 @	4.1	1290	2	-
SALT RIVER AT SHEPHERDSVILLE	0		@	8		(9)	
SALT RIVER AT SHEPHERDSVILLE	@	0		8			
SALT RIVER AT SHEPHERDSVILLE	14 @	32.6	36	4.4	1260	2	1
SALT RIVER AT SHEPHERDSVILLE	0			8	0		@
SALT RIVER AT SHEPHERDSVILLE	10 @		11	4.1	752 @	2 X	1
ROLLING FORK NEAR LEBANON JUNCTION	9		36 @	4	721 @	2	-
ROLLING FORK NEAR LEBANON JUNCTION	7 @		20 @		214 @		<u>-</u> ح
ROLLING FORK NEAR LEBANON JUNCTION	8		204 @	3.8	1880 @		<u>-</u>
ROLLING FORK NEAR LEBANON JUNCTION	9			3 @	1460 @		<u>←</u>
ROLLING FORK NEAR LEBANON JUNCTION	12 @		11 @	1.3 @	191 @	2 X	←
ROLLING FORK NEAR LEBANON JUNCTION		36	238 @	5.5	5250 @		7
ROLLING FORK NEAR LEBANON JUNCTION	5	35.2	11	2.6 @	394 @		<u>-</u>
ROLLING FORK NEAR LEBANON JUNCTION	4	10.4 @	236	3.3 @	5290 @	2	1 7
ROLLING FORK NEAR LEBANON JUNCTION	0			(9)	0		@
ROLLING FORK NEAR LEBANON JUNCTION	5 @	30.1@	160	(9)	2060 @	3	1 K
ROLLING FORK NEAR LEBANON JUNCTION				0	0	0	@
ROLLING FORK NEAR LEBANON JUNCTION	7 @	20.6 @	09	3.9 @	1910 @	2 @	1 K
ROLLING FORK NEAR LEBANON JUNCTION	0			0		@	0
ROLLING FORK NEAR LEBANON JUNCTION	7 @	2.09	2776	0.6 0.6	10800	9	<u>۔</u> ح
ROLLING FORK NEAR LEBANON JUNCTION	(B)			0	0		8
ROLLING FORK NEAR LEBANON JUNCTION				0	@		
ROLLING FORK NEAR LEBANON JUNCTION	10 @	61.2		4.1 @	337 @		<u>-</u>
ROLLING FORK NEAR LEBANON JUNCTION		59.5		4 @	@ 09E	2 K	<u>구</u>
ROLLING FORK NEAR LEBANON JUNCTION				2 @			1 X
ROLLING FORK NEAR LEBANON JUNCTION		43.9	137 @		1910 @	2 K	1 K
KOLLING FORK NEAR LEBANON JUNCTION	9	57.8	52 @	1.9@	997 @	2 K	<u>-</u>

LOCATION	940		946		530	-	089	-	1105		1002	-	1027	L
	CHLORIDE	Ø	SULFATE	2	RESIDUE	_	T ORG C	٩	ALUMINUM		ARSENIC	ပ်	CADMIUM	
	TOTAL	(O)	S04-DISS	H	TOT NFLT	ပ		٩	AL,TOT		AS,TOT	占	CD,TOT	_
	MG/L	2	MG/L	2	MG/L	2	MG/L	<u> </u>	UG/L		UG/L	UG/L	3/L	
ROLLING FORK NEAR LEBANON JUNCTION	3	(9)	25.3	(9)	72 ((a)	2.4	@		@	2 K		1	1 X
ROLLING FORK NEAR LEBANON JUNCTION	9	0	50.2	@	26 (0	2	@	521	®	2 K		1	7
ROLLING FORK NEAR LEBANON JUNCTION		@		@)	@		@		0	9	9		0
ROLLING FORK NEAR LEBANON JUNCTION	2	0	40.5	@	37 (@	2.9	0	169	(9)	2 K		1	노
ROLLING FORK NEAR LEBANON JUNCTION	ε	0	44.7	@	40	@	3		719	(9)	2 K		1	쏘
ROLLING FORK NEAR LEBANON JUNCTION	2	@	12.3	@	220	@	7.5	@	4430	@	2 K		1	¥
ROLLING FORK NEAR LEBANON JUNCTION	2	@	12.5	@	240	@	2.8	(a)	4830	(9)	2 @	9	1	1 K
ROLLING FORK NEAR LEBANON JUNCTION		0		©)	@		@	-	(0)	9	(a)		@
ROLLING FORK NEAR LEBANON JUNCTION	10	a	24.2	@	73	0	2.8	@	1210	@	3 @	(3)		¥
ROLLING FORK NEAR LEBANON JUNCTION		0		@)	@		@		@	0	@		0
ROLLING FORK NEAR LEBANON JUNCTION	6	@	56.9	@	86	@	3.5	@	1260	@	2 @	(S)		ᅩ
ROLLING FORK NEAR LEBANON JUNCTION		@		@)	0		0		@	9	@		9
ROLLING FORK NEAR LEBANON JUNCTION		0		@		@		@		0	<u> </u>	@		0
ROLLING FORK NEAR LEBANON JUNCTION	18	a	25.5	a	44	ම	3.3	@	828	@	2 @	@	•	ᅩ
ROLLING FORK NEAR LEBANON JUNCTION		@		@		@		@		@	9	@		0
ROLLING FORK NEAR LEBANON JUNCTION	23	@	24.6	@	8	ම	3.9	0	284 @	®	2 K		`	쏘
ROLLING FORK NEAR LEBANON JUNCTION	15	®	33.3	@	1	メ	-	®	253 @	®	2 K		•	ㅗ
ROLLING FORK NEAR LEBANON JUNCTION	8	@	33	@	13	@	3.1	@	311		2 K)	•	쏘
ROLLING FORK NEAR LEBANON JUNCTION		(9)		(6)		(9)		(0)		(B)	9	(a)		9
ROLLING FORK NEAR LEBANON JUNCTION	8	a	33	(9)	13	(9)	3.1	®	$\overline{}$	(9)	2 X		`	ㅗ
ROLLING FORK NEAR LEBANON JUNCTION	7	@	32	(9)		@	2.3	(9)	627	(9)	2 K		•	ㅗ
ROLLING FORK NEAR LEBANON JUNCTION	6	(0)	32.5	(9)	78	®	2.1	(a)	476	(9)	2 K		Ì	ㅗ
ROLLING FORK NEAR LEBANON JUNCTION	4	@	31	(9)	3800	(9)	6.1	(9)	2670	(9)	2 K			ᅩ
ROLLING FORK NEAR LEBANON JUNCTION	4	(9)	31	(B)	472	(a)	7.4	(0)	10300	(9)	2 X		•	ㅗ
ROLLING FORK NEAR LEBANON JUNCTION	3	a	9	(a)	320	a	5.8	(0)	2720	(9)	3	(a)		뇓
ROLLING FORK NEAR LEBANON JUNCTION		(a)		(B)		(0)		(9)				(a)		0
ROLLING FORK NEAR LEBANON JUNCTION	6	(9)	14.2	(B)	22	ම	3.7	(9)	1690	(9)	2 K			논
ROLLING FORK NEAR LEBANON JUNCTION		@		®		(0)		(9)		(6)	9	(a)		(0)
ROLLING FORK NEAR LEBANON JUNCTION		(0)		(a)		(0)		(9)		(9)		(a)		0
ROLLING FORK NEAR LEBANON JUNCTION	10	a	17.3	(9)	31	0	4.9	(9)	1070		2 X	_		౼
ROLLING FORK NEAR LEBANON JUNCTION		(0)		(0)		(a)		(9)		(9)	9	(a)		0
ROLLING FORK NEAR LEBANON JUNCTION	9	0	34.1	©	26	®	4.7	0	1090	(0)	2 k			늰

			040	200	1055	1300	1092	_
	CHROMIUM	COPPER	IRON	LEAD	MANGNESE	MERCURY	ZINC	
	тот	CU,TOT	FE,TOT	PB,TOT	Z	HG,TOTAL	ZN,TOT	
SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE		UG/L	UG/L	UG/L	UG/L	NG/L	UG/L	T
SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE	5 @	3 @	g 1070 @		129	@ 0.1 K	4	(9)
SALT RIVER AT SHEPHERDSVILLE SALT RIVER AT SHEPHERDSVILLE	<u>-</u>	<u>-</u>	734 @		85	@ 0.1 K	2	
SALT RIVER AT SHEPHERDSVILLE	-	2 @			117	@ 0.1 K	5	(9)
	5	4	ဗ		330	@ 0.1 K	11	(9)
SALT RIVER AT SHEPHERDSVILLE	<u>구</u>	1 @		2	33	@ 7 T.0	2	(9)
SALT RIVER AT SHEPHERDSVILLE	1 X	1 X			62		3	@
SALT RIVER AT SHEPHERDSVILLE	2 @	1 @			109	@ 0.1 K	3	(e)
SALT RIVER AT SHEPHERDSVILLE	1 K	1 K				0.1	4	(G)
SALT RIVER AT SHEPHERDSVILLE	@ 9	@ 6			263 @		2	
SALT RIVER AT SHEPHERDSVILLE	@	0	(9)				@	(8)
SALT RIVER AT SHEPHERDSVILLE	2 @	1 @	2690	3	202	0.1 K	8	(8)
SALT RIVER AT SHEPHERDSVILLE	@	(a)	(a)	8				(e)
SALT RIVER AT SHEPHERDSVILLE	2 @	2 @	1420	2	170	0.1	2	(B)
SALT RIVER AT SHEPHERDSVILLE	0	0						6
SALT RIVER AT SHEPHERDSVILLE	7	2 @	1290	2	122	0.1	8	V @
SALT RIVER AT SHEPHERDSVILLE	(B)	0				(a)) a
SALT RIVER AT SHEPHERDSVILLE	100	1 @	964	2	123	0.1	5	(a)
SALT RIVER AT SHEPHERDSVILLE	10	1	_		127	@ 7 L.0	4	(8)
SALT RIVER AT SHEPHERDSVILLE	1 @	1			87		2	
SALT RIVER AT SHEPHERDSVILLE	1 X	*	739		48		10	(8)
SALT RIVER AT SHEPHERDSVILLE	3 @	3 @	2630		166	@ 71.0		
SALT RIVER AT SHEPHERDSVILLE	2 @	@ 9	3320 @	3@	129	0.05	12	
SALT RIVER AT SHEPHERDSVILLE	1 X	1 @	920	2	100	© 0.05 K	4	0
SALT RIVER AT SHEPHERDSVILLE	(G)	<u> </u>		(a)				
SALT RIVER AT SHEPHERDSVILLE	-	1 @		2	86	0.05	2	
SALT RIVER AT SHEPHERDSVILLE	3	2 @	4390 @		2810	@ 0.05 K	12	
SALT RIVER AT SHEPHERDSVILLE	(9)	0	(0)	@				(0)
SALT RIVER AT SHEPHERDSVILLE	<u> </u>	1 @	209		47	0.05	2	
SALT RIVER AT SHEPHERDSVILLE	0	@					@	(0)
SALT RIVER AT SHEPHERDSVILLE	2 @	2 @	1130	2 K	117	@ 0.05 K	3	
SALT RIVER AT SHEPHERDSVILLE	@	0						
SALT RIVER AT SHEPHERDSVILLE	@	0						
SALT RIVER AT SHEPHERDSVILLE	<u>구</u>	1	245	2	33 (6	0.05	2	
SALT RIVER AT SHEPHERDSVILLE	(9)	8		@	9	@ @		
SALT RIVER AT SHEPHERDSVILLE	, 고	1 @	999	2 K	155	@ 0.05 K	3 @	

LOCATION	1034	1042	1045	1051	1055		71900	1092	32
	CHROMIUM	COPPER	IRON	LEAD	MANGNESE	Σ	MERCURY	ZINC	
	CR,TOT	CU,TOT	FE,TOT	PB,TOT	Z	Ĭ	HG,TOTAL	ZN,TOT	ĭ
	UG/L	UG/L	UG/L	NG/L	UG/L	Ď	NG/L	NG/L	
SALT RIVER AT SHEPHERDSVILLE	111	X 1 X		2 K	27	(a)	0.05 K		3@
SALT RIVER AT SHEPHERDSVILLE	111		401 @	2 K	54	®	0.05 K		2 ス
SALT RIVER AT SHEPHERDSVILLE	11		441 @	3@	43	@	0.05 K		3 (0)
SALT RIVER AT SHEPHERDSVILLE	1 K	1	929	2 K	59	(9)	0.05 K		
SALT RIVER AT SHEPHERDSVILLE	2 (@ 2@	1590	2 K	108	@	0.05 K		12@
SALT RIVER AT SHEPHERDSVILLE	5 (6 5 6	g 4530 @	7 @	382	ම	0.05 K		36 @
SALT RIVER AT SHEPHERDSVILLE	2 (0 2 0	2080	2 @	192	@	0.05 K		006
SALT RIVER AT SHEPHERDSVILLE		@ @				@	<u>@</u>	í	0
SALT RIVER AT SHEPHERDSVILLE	-	2	1570	2	163	ම	0.05 K		8 K
SALT RIVER AT SHEPHERDSVILLE		@ @	(a)			@	0	Č	9
SALT RIVER AT SHEPHERDSVILLE)			@		(a)	0	0	(9)
SALT RIVER AT SHEPHERDSVILLE	2 (2	1520 @	2	149	@	0.05 K		8 ⊼
SALT RIVER AT SHEPHERDSVILLE			@ @			@	0)	0
SALT RIVER AT SHEPHERDSVILLE	-	1	096		101	<u>_</u>	0.05 K		5 K
ROLLING FORK NEAR LEBANON JUNCTION	2 @	2	1600		82	(B)	0.1 K		4
ROLLING FORK NEAR LEBANON JUNCTION	1 7	-	649		54	@	0.1 K		2 K
ROLLING FORK NEAR LEBANON JUNCTION	1 K	4	@ 3480 @	5 @	198	(a)	0.1 K		12@
ROLLING FORK NEAR LEBANON JUNCTION	4 (3 (2340		163	(9)	0.1 K		13
ROLLING FORK NEAR LEBANON JUNCTION	1	1	604		52	(a)	0.1 X		
ROLLING FORK NEAR LEBANON JUNCTION)	9 @	9480	5	267	(B)	0.1 K		25 @
ROLLING FORK NEAR LEBANON JUNCTION	1	1	@ 121 @	2	44	@	0.1 K		5 @
ROLLING FORK NEAR LEBANON JUNCTION	9	0 0	9020	9	253	@	0.1 K		2 K
ROLLING FORK NEAR LEBANON JUNCTION		@	@ @		0	0	0	0	0
ROLLING FORK NEAR LEBANON JUNCTION	9	0 2	3940	4	158	(6)	0.1 K	-	13@
ROLLING FORK NEAR LEBANON JUNCTION		0			(8)	(9)	0	(2)	9
ROLLING FORK NEAR LEBANON JUNCTION	2	3	@ 3110@	2	114	(a)	0.1 X		8
ROLLING FORK NEAR LEBANON JUNCTION					9	@	0	0	•
ROLLING FORK NEAR LEBANON JUNCTION	1	K 13 (@ 22300@	17	@ 585	(9)	0.1 X		45 @
ROLLING FORK NEAR LEBANON JUNCTION					©	(9)	0	((a)
ROLLING FORK NEAR LEBANON JUNCTION			0		(9)	(0)	0	(2)	<u>@</u>
ROLLING FORK NEAR LEBANON JUNCTION	1	K 2 (73	(9)	0.1 X		<u>9</u>
ROLLING FORK NEAR LEBANON JUNCTION	1 K	1	@ 008 @	2 K	48	(a)	0.1 K		5
ROLLING FORK NEAR LEBANON JUNCTION	_	_	1320	2	63				2
ROLLING FORK NEAR LEBANON JUNCTION	4	3		3	144		0.1 X		13
ROLLING FORK NEAR LEBANON JUNCTION	_	0 1 (@ 1850@	2	77	(9)	0.1 K		8

LOCATION	1034	1042	1045	1051	1055	71900	1092
	CHROMIUM	COPPER	IRON	LEAD	MANGNESE	MERCURY	ZINC
	CR,TOT	CU,TOT	FE,TOT	PB,TOT	Z	HG,TOTAL	ZN,TOT
To grant the state of the state	UG/L	NG/L	NG/L	UG/L	UG/L	UG/L	UG/L
ROLLING FORK NEAR LEBANON JUNCTION	1	@ 2@	2130 @	2 X	106	@ 0.05 K	12 @
ROLLING FORK NEAR LEBANON JUNCTION	<u>1</u> ح	1 @	1340 @	2 K	126 @	9 0.05 K	5
ROLLING FORK NEAR LEBANON JUNCTION	9	0	0	(B)		8	
ROLLING FORK NEAR LEBANON JUNCTION	-	0 2 0	1500 @	2 K	102 @	9 0.05 K	5
ROLLING FORK NEAR LEBANON JUNCTION	1	0 2 @	@ 800 @	2 K	87 @	9 0.05 K	4
ROLLING FORK NEAR LEBANON JUNCTION	5 (6	@ 4 @	@ 9020 @	4	240 @	0.05 K	21 @
ROLLING FORK NEAR LEBANON JUNCTION	@ 9	0 2 0	9240	5	258 @	0.05 K	22 @
ROLLING FORK NEAR LEBANON JUNCTION	0	@	0	(B)	8	(9)	
ROLLING FORK NEAR LEBANON JUNCTION	3@	2 @	2170 @	@ E	123 @	0.05 K	5 @
ROLLING FORK NEAR LEBANON JUNCTION	0	0	0	@	(8)	(9)	
ROLLING FORK NEAR LEBANON JUNCTION	3	3 @	2380 @	3@	180 @	9 0.05 K	9
ROLLING FORK NEAR LEBANON JUNCTION	0			0	(1)	(9)	
ROLLING FORK NEAR LEBANON JUNCTION	0	0		®			
ROLLING FORK NEAR LEBANON JUNCTION	2 @	1 @	1700 @	3	194 @	0.05 K	2
ROLLING FORK NEAR LEBANON JUNCTION	0		@	®	(3)	(9)	
ROLLING FORK NEAR LEBANON JUNCTION	7	1	841 @	2 K	305 @	0.05 K	2 @
ROLLING FORK NEAR LEBANON JUNCTION	<u>۔</u> ح	1 @	934 @	2 K	© 66	0.05 K	2 @
ROLLING FORK NEAR LEBANON JUNCTION	1- X	1 @		2 K	48	0.05 K	
ROLLING FORK NEAR LEBANON JUNCTION	0			0	(B)	0	(9)
ROLLING FORK NEAR LEBANON JUNCTION	<u>←</u>	-	726 @	2 K	48 @	0.05	2 X
ROLLING FORK NEAR LEBANON JUNCTION		7		3@	<u>ම</u> 69	0.05 K	4
ROLLING FORK NEAR LEBANON JUNCTION	<u></u>	-		2 K	@ 09	0.05 K	4 @
ROLLING FORK NEAR LEBANON JUNCTION		8	_	9	343 @	0.05 K	45 @
ROLLING FORK NEAR LEBANON JUNCTION		7	20700	<u>®</u>	299 @		55 @
ROLLING FORK NEAR LEBANON JUNCTION	9	5	4360	8	348 @	0.05 K	19 @
ROLLING FORK NEAR LEBANON JUNCTION	_			0	0	0	<u>@</u>
ROLLING FORK NEAR LEBANON JUNCTION	2 @	ဇ	2500 @	2 7	126 @	0.05 K	8 K
ROLLING FORK NEAR LEBANON JUNCTION	0			0	0	0	@
ROLLING FORK NEAR LEBANON JUNCTION				0	0	0	@
ROLLING FORK NEAR LEBANON JUNCTION	2 @	2	1630	2 X	121 @	0.05 K	8 K
ROLLING FORK NEAR LEBANON JUNCTION	®	(0)		0	0		®
ROLLING FORK NEAR LEBANON JUNCTION	<u>ナ</u>		1670 @	2K	83 @	0.05 K	8 K

LOCATION	916	927	937	926	006	610	920
	CALCIUM	MGNSIUM	PTSSIUM	SODIUM	TOT HARD	NH3+NH4-	NO2&NO3
	CA-TOT	MG,TOT	K,TOT	NA,TOT	CACO3	N TOTAL	N-TOTAL
	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L	MG/L
SALT RIVER AT SHEPHERDSVILLE	53.5		@ 6.24 (@ 12.2 @	@ 183	@	1.27
SALT RIVER AT SHEPHERDSVILLE	60.3	9.4	3.54 ((8)	@ 0.166	1.13@
SALT RIVER AT SHEPHERDSVILLE	61.1	13.7 (3.72 (@ 7.62 (@ 209	@	1.68
SALT RIVER AT SHEPHERDSVILLE	61.6	0 11.3	3.01	9.61	@ 200	0.065	
SALT RIVER AT SHEPHERDSVILLE	6.89	0.01	2.45	7.74	@ 217	@ 0.05 K	
SALT RIVER AT SHEPHERDSVILLE	66.3	11.2	2.14	@ 6.41	@ 212	@	1.54 @
SALT RIVER AT SHEPHERDSVILLE	63.3	11.6	@ 2.83	@ 6.43	@ 206	@ 0.05 K	
SALT RIVER AT SHEPHERDSVILLE	56.3	9.4	@ 2.15 (0 179	(B)	
SALT RIVER AT SHEPHERDSVILLE	61.1 @	10.4	3.09 (3.48	0 195	@ 0.05 K	(1.22 @
SALT RIVER AT SHEPHERDSVILLE		8	(9)	(a)	@	<u></u>	@ @
SALT RIVER AT SHEPHERDSVILLE	47.5	@ 5.7	3.34	3.39	0 142	@ 0.05 K	0.44
SALT RIVER AT SHEPHERDSVILLE					@		
SALT RIVER AT SHEPHERDSVILLE	46.2	0 7.5	4.11	6.03	@ 146	@ 0.052	0.6@
SALT RIVER AT SHEPHERDSVILLE		(a)) @	0	@	0	@ @
SALT RIVER AT SHEPHERDSVILLE	45.8	@ 8.7	3.66	@ 7.76 (@ 150	@ 0.05 K	د 0.74 @
SALT RIVER AT SHEPHERDSVILLE		@	(@) @	@	@	-
SALT RIVER AT SHEPHERDSVILLE	64.3	0 14.5	@ 4.7	0 10.4	@ 220	ම	
SALT RIVER AT SHEPHERDSVILLE	26.3	2 @	3.34		@ 169	©	
SALT RIVER AT SHEPHERDSVILLE	61.8	8 @	3.24		@ 187	@ 0.05 K	
SALT RIVER AT SHEPHERDSVILLE	9.79	0 11.6			@ 216	(B)	
SALT RIVER AT SHEPHERDSVILLE	53 (0 2		3.57 (0 161	@ 0.05 K	
SALT RIVER AT SHEPHERDSVILLE	41.3	0 2.9	@ 2.34	@ 2.73 ((0) 127	(B)	
SALT RIVER AT SHEPHERDSVILLE	9.69	0 14.8	@ 2.57		@ 235	@ 0.05 K	K 0.37 @
SALT RIVER AT SHEPHERDSVILLE		@	_	@	(B)	0)	0
SALT RIVER AT SHEPHERDSVILLE	61.6	0 11.6				@ 0.05	0.85
SALT RIVER AT SHEPHERDSVILLE	62.2	6.8	@ 2.8	3.06 ((0) 192	@ 0.05	1.64
SALT RIVER AT SHEPHERDSVILLE		0	@	(0)	©	®	
SALT RIVER AT SHEPHERDSVILLE	58.4	10.1	3.08	@ 7.03	(0) 187	0.075	@ 0.39 @
SALT RIVER AT SHEPHERDSVILLE		0	0	@	©		(a) (b)
SALT RIVER AT SHEPHERDSVILLE	50.1	0 14.5	@ 4.43	12.3	(0) 185	0.094	1.2
SALT RIVER AT SHEPHERDSVILLE					®		
SALT RIVER AT SHEPHERDSVILLE		©	(9)	8		©	<u> </u>
SALT RIVER AT SHEPHERDSVILLE	45.8	(0) 12	4.15	14.8	164	@ 0.05	0.72
SALT RIVER AT SHEPHERDSVILLE						@	
SALT RIVER AT SHEPHERDSVILLE	57.2	(3.2	4.07	(0) 17.3	(@) 197	0.074	@ 0.43@

LOCATION	916	927		937	929	006		610	630	
	CALCIUM	MGNSIOM	PTS	PTSSIUM	SODIUM	TOT HARD	Z	NH3+NH4-	NO2&NO3	
	CA-TOT	MG,TOT	K,TOT	ОТ	NA,TOT	CACO3	Z	N TOTAL	N-TOTAL	
	MG/L	MG/L	MG/L	/r	MG/L	MG/L	Σ	MG/L	MG/L	
SALT RIVER AT SHEPHERDSVILLE		@ 5.5	@	2.15 @	4.81	@ 70	(9)	0.05 K	0.11	(9)
SALT RIVER AT SHEPHERDSVILLE		11	(B)	3.17 @	8.82	0 192 @	(9)	0.05 K	1.31	(9)
SALT RIVER AT SHEPHERDSVILLE	$\overline{}$	11.7	©	2.41		@ 216 @	@	0.05 K	2.02	(9)
SALT RIVER AT SHEPHERDSVILLE	_		(a)	2.23 @	7.08	@ 233 @	@	0.05 K	1.14	(9)
SALT RIVER AT SHEPHERDSVILLE		00 10.6	@	2.34 @		0 171	(9)	0.05 K	69.0	(9)
SALT RIVER AT SHEPHERDSVILLE		9.6	@	3.26		133		0.09	0.72	(9)
SALT RIVER AT SHEPHERDSVILLE	9.69	8.4	@	2.85 @		11		0.05 K	1.06	0
SALT RIVER AT SHEPHERDSVILLE	9	0	@	0	9	0	(9)	(a)		(9)
SALT RIVER AT SHEPHERDSVILLE	57.2 (12.5	@	3.7 @	6.42	194	(9)	0.05 K	0.75	(9)
SALT RIVER AT SHEPHERDSVILLE		0	@	0		@	®	(8)		(9)
SALT RIVER AT SHEPHERDSVILLE	•	0	@	@		@	(9)	(G)		(8)
SALT RIVER AT SHEPHERDSVILLE	44.8	10.1	(B)	4.49 @	9.68	@ 153		0.05 K	9.0	(0)
SALT RIVER AT SHEPHERDSVILLE			(a)	0	9	@	(a)	(9)		(9)
SALT RIVER AT SHEPHERDSVILLE		8.8	(a)	3.18		168		0.05 K	1.13	(9)
ROLLING FORK NEAR LEBANON JUNCTION	47.4 (©			157	®	0.05 K	0.95	(9)
ROLLING FORK NEAR LEBANON JUNCTION	29 @		(B)	2.84 @	4.03	00 199	@	0.05 K	1.29	(0)
ROLLING FORK NEAR LEBANON JUNCTION	53.9 @		(a)	3.19@		194	0	0.05 K	0.72	(9)
ROLLING FORK NEAR LEBANON JUNCTION	57 @		(B)	2.52 @	4.59 @		@	0.05 K	1.31	(9)
ROLLING FORK NEAR LEBANON JUNCTION	61.9@	12.8	(B)	1.79 @	5.02 @		@	0.05 K	1.32	(9)
ROLLING FORK NEAR LEBANON JUNCTION	44.8 @	10	(9)	3.38 @	3.49 @	153	@	0.05@	0.71	(9)
ROLLING FORK NEAR LEBANON JUNCTION	59.9	12.3	®		3.51 @	200	@	0.052@	1.01	(9)
ROLLING FORK NEAR LEBANON JUNCTION	45 @	9.5	(9)	3.32 @	2.15 @	150		0.05 K	96.0	(9)
ROLLING FORK NEAR LEBANON JUNCTION			(a)	(B)	9	(0)	@	@		(9)
ROLLING FORK NEAR LEBANON JUNCTION	43.1	8.1	®	3.63 @	2.95 @	141	(9)	0.05 K	1.21	@
ROLLING FORK NEAR LEBANON JUNCTION			(a)					0		@
ROLLING FORK NEAR LEBANON JUNCTION	44.6 @	6.6	®	4.11	4.51 @	152		0.05 K	0.53	@
ROLLING FORK NEAR LEBANON JUNCTION			®				(9)	0		(6)
ROLLING FORK NEAR LEBANON JUNCTION	53.3 @	10.1	®	4.19 @	4.83 @	175	@	0.113	89.0	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0		(a)	(9)	0	0	(a)	@		(9)
ROLLING FORK NEAR LEBANON JUNCTION			(a)		0		(a)	@		(9)
ROLLING FORK NEAR LEBANON JUNCTION	58.2 @		0	3.9		203	@	0.05 K		(9)
ROLLING FORK NEAR LEBANON JUNCTION	64.1		(a)	3.15 @		207	(B)	0.05 K	0.88	a
ROLLING FORK NEAR LEBANON JUNCTION	65.9		(9)	2.4 @	4.31		@	0.05 K	1.28	(a)
ROLLING FORK NEAR LEBANON JUNCTION	62 @	13.7	a	2.13 @	5.59 @		®	0.05 K	0.96	(9)
ROLLING FORK NEAR LEBANON JUNCTION	57.9 @	11.9	©	1.87	3.48 @	194 @	(a)	0.05 K	1.38	(8)

LOCATION	916	927	Ĺ	937	-	929	6	006	610		930	Γ
	CALCIUM	MGNSIUM		PTSSIUM	S	SODIUM	TOT HARD	Q	NH3+NH4-		NO2&NO3	
	CA-TOT	MG,TOT		K,TOT	₹	NA,TOT	CACO3		N TOTAL		N-TOTAL	
1250	MG/L	MG/L		MG/L	MG/L	;/L	MG/L		MG/L		MG/L	
ROLLING FORK NEAR LEBANON JUNCTION	50.3	10.8	®	1.79 (@	3.08 @		170 @		¥	0.97	(9)
ROLLING FORK NEAR LEBANON JUNCTION	71.7 (18.1	0	2.26	(B)	5.94 @		254 @	0.05	¥	0.13	(9)
ROLLING FORK NEAR LEBANON JUNCTION		®	0)	©	0		(8)		(9)		(a)
ROLLING FORK NEAR LEBANON JUNCTION	55.8	0 11.8	@	2.1	@	4.23 @		188 @	0.05	노	0.32	9
ROLLING FORK NEAR LEBANON JUNCTION	50.5	0 11.6	@	2.17 (@	4.31		174 @		노	0.31	(9)
ROLLING FORK NEAR LEBANON JUNCTION	31.9	@ 5.9	<u>@</u>	2.61	@	1.37 @		104 @	0.05 K	노	0.7	(B)
ROLLING FORK NEAR LEBANON JUNCTION	35.1 (@ 6.5	.e	2.84 (@	1.49 @		114 @	0.05	ㅈ	0.69	
ROLLING FORK NEAR LEBANON JUNCTION		®	9)	0	©		(9)	0	(9)		(0)
ROLLING FORK NEAR LEBANON JUNCTION	62.4	13.9	@	2.85 (@	9.9		213 @	0.09	(9)	0.57	(B)
ROLLING FORK NEAR LEBANON JUNCTION		@	@)	@	@	0	(0)	0)	(9)		(0)
ROLLING FORK NEAR LEBANON JUNCTION	53.3	@ 15.8	3 @	3.4 (@	6.68		198 @	0.05	ㅈ	0.46	(9)
ROLLING FORK NEAR LEBANON JUNCTION		@	@	<u> </u>	@	©	Õ	(0)	0	(9)		(9)
ROLLING FORK NEAR LEBANON JUNCTION		@	@		@	©	0	(0)		(9)		(9)
ROLLING FORK NEAR LEBANON JUNCTION	64	@ 16.8	@	3.71	®	11.9 @		229 @	0.079	(0)	0.25	(9)
ROLLING FORK NEAR LEBANON JUNCTION		0	@)	®	(a)	0	(0)		(9)		(9)
ROLLING FORK NEAR LEBANON JUNCTION	73.2	0 17.5	9	3.74	@	15.2 @			0	<u> </u>	0.05	(0)
ROLLING FORK NEAR LEBANON JUNCTION	53 ((0) 14.3	3 @	3.67	®	10.8		191	0.05	χ Σ	0.41	9
ROLLING FORK NEAR LEBANON JUNCTION	55.5	11.4	9	2.58	@	4.51 @		186 @	0.05	ㅈ	1.94	(9)
ROLLING FORK NEAR LEBANON JUNCTION		8	(0)		(a)	@				(9)		
ROLLING FORK NEAR LEBANON JUNCTION	55.5	11.4	4 @		(9)	4.51 @					1.94	(9)
ROLLING FORK NEAR LEBANON JUNCTION	64.9	@ 13.4	9	2.23	(B)					소	1.5	
ROLLING FORK NEAR LEBANON JUNCTION	9:55	12.1	100	1.9	(B)	4.21 @					0.67	(8)
ROLLING FORK NEAR LEBANON JUNCTION	38.1	0 11.4	9		(B)			142			0.42	
ROLLING FORK NEAR LEBANON JUNCTION	53.5	0 17.4	4		(B)	3.37 @		-	0		0.38	
ROLLING FORK NEAR LEBANON JUNCTION	39.2		9	3.23	(a)	1.86		127	@ 0.05		0.17	-
ROLLING FORK NEAR LEBANON JUNCTION		@	(0)		(9)					\rightarrow		
ROLLING FORK NEAR LEBANON JUNCTION	53.6	12.	<u>@</u> 6	4.18	(a)	6.52 @		187	@ 0.055	_	0.63	
ROLLING FORK NEAR LEBANON JUNCTION		0	@		(a)	(0)	0		©	@		(0)
ROLLING FORK NEAR LEBANON JUNCTION		©	@		(a)	0	(a)					
ROLLING FORK NEAR LEBANON JUNCTION	51	11.	8; (0)	4.65	(B)	6.45		176	0.05	=	0.73	
ROLLING FORK NEAR LEBANON JUNCTION		©	0		®	_				(0)		$\overline{}$
ROLLING FORK NEAR LEBANON JUNCTION	54.1	11.4	9	2.95	(e)	3.97 (6	(0)	182 (@ 0.05	실	1.27	9

	625		999	31616	9
	TOT KJEL	PHOS-TOT	TOT	FEC COLI	
	Z.			MFM-FCBR	~
	MG/L	MG/L P	-	/100ML	├
SALT RIVER AT SHEPHERDSVILLE	0.735@		0.25	0	0
SALT RIVER AT SHEPHERDSVILLE	0.675		0.116@	0	0
SALT RIVER AT SHEPHERDSVILLE	0.602		0.232@		@
SALT RIVER AT SHEPHERDSVILLE	1.02 @		0.431	0	0
SALT RIVER AT SHEPHERDSVILLE	0.464		0.108@	0	0
SALT RIVER AT SHEPHERDSVILLE	0.679		0.117 @	0	@
SALT RIVER AT SHEPHERDSVILLE	0.869		0.233 @	0	6
SALT RIVER AT SHEPHERDSVILLE	0.368		0.114	099	
	0.889		0.348	220	
	0	0)	@	1600	@ 0
SALT RIVER AT SHEPHERDSVILLE	0.723 @		0.218		(0)
SALT RIVER AT SHEPHERDSVILLE	@	<u> </u>	®	0096	
SALT RIVER AT SHEPHERDSVILLE	0.75 @		0.17		(9)
SALT RIVER AT SHEPHERDSVILLE	0	0	(0)		10@
SALT RIVER AT SHEPHERDSVILLE	0.623 @		0.191		6
	0	Õ	(0)	200	
SALT RIVER AT SHEPHERDSVILLE	0.709		0.193@		0
SALT RIVER AT SHEPHERDSVILLE	0.482 @		0.108@		(0)
SALT RIVER AT SHEPHERDSVILLE	0.725 @		0.101 @		(9)
SALT RIVER AT SHEPHERDSVILLE	0.504		0.127 @		(0)
SALT RIVER AT SHEPHERDSVILLE	0.499		0.257 @		(9)
SALT RIVER AT SHEPHERDSVILLE	0.48		0.304		(0)
	0.594		0.115@		0
			(B)	350	0
SAL I RIVER AT SHEPHERDSVILLE			0.113@		@
SALT RIVER AT SHEPHERDSVILLE	1.07 @		0.394		@
SAL I RIVER AT SHEPHERDSVILLE			@	2000	<u>@</u>
SAL I RIVER AT SHEPHERDSVILLE	0.726 @		0.1		(0)
SALT RIVER AT SHEPHERDSVILLE	0		0	1700	@
	0.552 @		0.141		0
	0		@	140	@
	(B)		(B)	20	@
SALT RIVER AT SHEPHERDSVILLE	0.626@		0.098		0
SALI RIVER AI SHEPHERDSVILLE				220	
SAL I RIVER AT SHEPHERDSVILLE	0.295@		0.081		0

Location	625	999	-	31616	Г
	TOT KJEL	PHOS-TOT	豆	FEC COLI	
	z		M	MFM-FCBR	
	MG/L	MG/L P	7	/100ML	
SALT RIVER AT SHEPHERDSVILLE	0.159 @	0.018	(9)		(0)
SALT RIVER AT SHEPHERDSVILLE	0.384		@		(0)
SALT RIVER AT SHEPHERDSVILLE	0.928		(0)		(9)
SALT RIVER AT SHEPHERDSVILLE	0.284		(0))	0
SALT RIVER AT SHEPHERDSVILLE	1.8	0.112	(0)	(0
SALT RIVER AT SHEPHERDSVILLE	1.32 @	0.211	@		@
SALT RIVER AT SHEPHERDSVILLE	0.834	0.204	@		0
SALT RIVER AT SHEPHERDSVILLE	0		(B)	12000	(9)
SALT RIVER AT SHEPHERDSVILLE	0.617	60.00	(9)		@
SALT RIVER AT SHEPHERDSVILLE	(a)		(9)	110	0
SALT RIVER AT SHEPHERDSVILLE	(B)		(9)	20	(9)
SALT RIVER AT SHEPHERDSVILLE	0.551	0.142	(9)		0
SALT RIVER AT SHEPHERDSVILLE	(a)		(9)	1000	0
SALT RIVER AT SHEPHERDSVILLE	0.388	0.101	@		@
ROLLING FORK NEAR LEBANON JUNCTION	0.602	0.112	@		0
ROLLING FORK NEAR LEBANON JUNCTION	0.478		(9)		(9)
ROLLING FORK NEAR LEBANON JUNCTION	1.05 @	0.255	(9)		a
ROLLING FORK NEAR LEBANON JUNCTION		0.216	(9)		@
ROLLING FORK NEAR LEBANON JUNCTION	0.335@		(9)		0
ROLLING FORK NEAR LEBANON JUNCTION	1.01 @				(9)
ROLLING FORK NEAR LEBANON JUNCTION	_			250	(0)
ROLLING FORK NEAR LEBANON JUNCTION	1.21 @	0.324	(9)	380	(9)
ROLLING FORK NEAR LEBANON JUNCTION	(9)	0	(B)	1100	9
ROLLING FORK NEAR LEBANON JUNCTION	1.56 @	0.19	(a)		@
ROLLING FORK NEAR LEBANON JUNCTION	®	0	(9)	250	@
ROLLING FORK NEAR LEBANON JUNCTION	0.829	0.109	(B)		(0)
ROLLING FORK NEAR LEBANON JUNCTION				170	@
ROLLING FORK NEAR LEBANON JUNCTION	1.86 @	0.534			@
ROLLING FORK NEAR LEBANON JUNCTION	0	0	(9)	120	@
ROLLING FORK NEAR LEBANON JUNCTION	0	0	@		@
ROLLING FORK NEAR LEBANON JUNCTION	0.334		(9)		(0)
ROLLING FORK NEAR LEBANON JUNCTION	0.334 @		(9)		@
ROLLING FORK NEAR LEBANON JUNCTION	0.175		(9)		@
ROLLING FORK NEAR LEBANON JUNCTION	1.01		(9)		@
ROLLING FORK NEAR LEBANON JUNCTION	0.204 @	0.075	@		@

LOCATION	625	999	31616	
	TOT KJEL	PHOS-TOT	FEC COLI	
	z		MFM-FCBR	
The state of the s	MG/L	MG/L P	/100ML	
ROLLING FORK NEAR LEBANON JUNCTION	0.743	0.092	8	(0)
ROLLING FORK NEAR LEBANON JUNCTION	0.388	0.039	(a)	(9)
ROLLING FORK NEAR LEBANON JUNCTION	©		230	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0.4	0.07	(a)	(0)
ROLLING FORK NEAR LEBANON JUNCTION	0.283 @	0.067	0	(9)
ROLLING FORK NEAR LEBANON JUNCTION	1.06 @	0.396	(9)	(0)
ROLLING FORK NEAR LEBANON JUNCTION	1.27 @	0.39	©	(0)
ROLLING FORK NEAR LEBANON JUNCTION	®		1400	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0.899	0.112	8	(9)
ROLLING FORK NEAR LEBANON JUNCTION	@	9	30	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0.539	0.01	©	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0	9	@ 240	(9)
ROLLING FORK NEAR LEBANON JUNCTION	@)	30	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0.283 @	0.068	0	®
ROLLING FORK NEAR LEBANON JUNCTION	(0)	9	110	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0.458 @	0.067	@	@
ROLLING FORK NEAR LEBANON JUNCTION	0.764	0.059	0	(g)
ROLLING FORK NEAR LEBANON JUNCTION	0.684	0.039	0	@
ROLLING FORK NEAR LEBANON JUNCTION		0	(9)	(a)
ROLLING FORK NEAR LEBANON JUNCTION			(B)	(B)
ROLLING FORK NEAR LEBANON JUNCTION			0	(0)
ROLLING FORK NEAR LEBANON JUNCTION	-			(9)
ROLLING FORK NEAR LEBANON JUNCTION	\rightarrow	0.316		(9)
ROLLING FORK NEAR LEBANON JUNCTION		0.419	(B)	(9)
ROLLING FORK NEAR LEBANON JUNCTION	0.821 @	0.418	0	@
ROLLING FORK NEAR LEBANON JUNCTION	®	0	1300	(g)
ROLLING FORK NEAR LEBANON JUNCTION	1.09 @	0.063	0	(9)
ROLLING FORK NEAR LEBANON JUNCTION	(9)	0	09 @	@
ROLLING FORK NEAR LEBANON JUNCTION	(B)	0	06	(0)
ROLLING FORK NEAR LEBANON JUNCTION	0.304 @	0.097 @		a
ROLLING FORK NEAR LEBANON JUNCTION		-,	09	®
ROLLING FORK NEAR LEBANON JUNCTION	0.382@	0.109@		(9)

Appendix C
Output from FLUX Applications
for the Salt River and Rolling
Fork River Calculation of Loading
Estimates for Total Nonfilterable
Residue Concentrations

Salt River VAR=totnflt METHOD= 2 Q WTD C COMPARISON OF SAMPLED AND TOTAL FLOW DISTRIBUTIONS STR NQ NC NE VOL% TOTAL FLOW SAMPLED FLOW C/Q SLOPE SIGNIF 1 747 22 22 15.5 466.690 474.880 .357 .027

2 429 13 13 84.5 4438.523 3449.683 *** 1176 35 35 100.0 1915.598 1579.807

FLOW STATISTICS

FLOW DURATION = 1176.0 DAYS = 3.220 YEARS

MEAN FLOW RATE = 1915.598 HM3/YR

TOTAL FLOW VOLUME = 6167.68 HM3

FLOW DATE RANGE = 19951012 TO 19981230 SAMPLE DATE RANGE = 19951012 TO 19981217

METHOD	MASS (KG)	FLUX (KG/YR)	FLUX VARIANCE	CONC (PPB)	CV
1 AV LOAD	413168300.0	128324600.0	.8377E+15	66989.29	.226
2 Q WTD C	521698600.0	162032700.0	.1050E+16	84585.92	.200
3 IJC	523557000.0	162609900.0	.1021E+16	84887.23	.197
4 REG-1	595510300.0	184957600.0	.1781E+16	96553.43	.228
5 REG-2	808612100.0	251144200.0	.3420E+17	131104.80	.736
6 REG-3	638657700.0	198358600.0	.2560E+16	103549.20	.255

Salt River

VAR=totnflt METHOD= 2 Q WTD C

.558

.469

FLUX Breakdown by Stratum:

			FREQ	FLOW	FLUX	VOLUME	MASS	CONC	CV
\mathtt{ST}	NS	NE	DAYS	HM3/YR	KG/YR	НМЗ	KG	PPB	_
1	22	22	747.0	466.69	15658980.0	954.46	32025350.0	33553.3	.388
2	13	13	429.0	4438.524	116907100.0	5213.21	489673200.0	93929.2	.212
***	35	35	1176.0	1915.60	62032700.0	6167.68	521698600.0	84585.9	.200

Optimal Sample Allocation:

ST	NS	NE	NE%	NEOPT%	FREQ%	VOL%	MASS%	VAR%	VARIANCE	CV
1	22	22	62.9	13.5	63.5	15.5	6.1	1.4	.1490E+14	.388
2	13	13	37.1	86.5	36.5	84.5	93.9	98.6	.1035E+16	.212
***	35	35	100.0	100.0	100.0	100.0	100.0	100.0	.1050E+16	.200

Optimal Allocation of 35 Sampled Events Across Strata (According to NEOPT%) Would Reduce CV of FLUX Estimate from .200 to .140

Rollin COMPAR		SAM	PLED	AND T	VAR=to	otnflt STRIBUTIO		= 2 Ç	O TTW C	2
STR				VOL%	TOTAL FLOW			C/Q	SLOPE	SIGNIF
1	-			21.2	579.034	632	2.101		.225	.285
2	287			78.8	6647.074	7280	0.676	-	-1.160	.303
***	1176	34	34	100.0	2059.925	1805	5.379			

FLOW STATISTICS

1176.0 DAYS = 3.220 YEARS

FLOW DURATION = 1176.0 DAYS = MEAN FLOW RATE = 2059.925 HM3/YR

TOTAL FLOW VOLUME = 6632.37 HM3

FLOW DATE RANGE = 19951012 TO 19981230 SAMPLE DATE RANGE = 19951012 TO 19981217

METHOD	MASS (KG)	FLUX (KG/YR)	FLUX VARIANCE	CONC (PPB)	CV
1 AV LOAD	2499837000.0	776416200.0	.8780E+17	376914.80	.382
2 O WTD C	2282719000.0	708982200.0	.1053E+18	344178.70	.458
3 IJC	2110852000.0	655602500.0	.6776E+17	318265.30	.397
4 REG-1	2520173000.0	782732300.0	.1889E+18	379981.00	.555
5 REG-2	2624965000.0	815279300.0	.1758E+18	395781.10	.514
6 REG-3	4386940000.0	1362525000.0	.1281E+19	661444.30	.831

Rolling Fork

VAR=totnflt METHOD= 2 Q WTD C

FLUX Breakdown by Stratum:

			FREO	FLOW	${ t FLUX}$	VOLUME	MASS	CONC	CV
ST	NS	NE	DAYS	HM3/YR	KG/YR	нмз	KG	PPB	-
1	28	28	889.0	579.03	52759060.0	1409.34	128412900.0	91115.6	.314
2	6	6	287.0	6647.07	****	5223.032	2154306000.0	412463.2	.485
***	34	34	1176.0	2059.92	708982200.0	6632.372	2282719000.0	344178.7	.458

Optimal Sample Allocation:

ST	NS	NE	NE%	NEOPT%	FREO%	VOL%	MASS%	VAR%	VARIANCE	CV
1									.1567E+15	
		-6	17.6	92.3	24.4	78.8	94.4	99.9	.1052E+18	.485
***	34	34	100.0	100.0	100.0	100.0	100.0	100.0	.1053E+18	.458

Optimal Allocation of 34 Sampled Events Across Strata (According to NEOPT%) Would Reduce CV of FLUX Estimate from .458 to .208

REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC20503.

1.AGENCY USE ONLY (Leave blank)

2.REPORT DATE February 2001 **3.REPORT TYPE AND DATES COVERED**

Final report

4.TITLE AND SUBTITLE

Water Quality and Potential Sediment Erosion Assessment for Proposed

Construction at Fort Knox, Kentucky

6.AUTHOR(S)

Steven L. Ashby, William D. Martin, Cassandra N. Gaines

7.PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)

U.S. Army Engineer Research and Development Center, Environmental Laboratory and Coastal and Hydraulics Laboratory,

3909 Halls Ferry Road, Vicksburg, MS 39180-6199

9.SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)

Directorate of Base Operations Support, 1110B 6th Avenue, Fort Knox, KY 40121-5000

8.PERFORMING ORGANIZATION REPORT NUMBER ERDC SR-01-1

5.FUNDING NUMBERS

10.SPONSORING/MONITORING **AGENCY REPORT NUMBER**

11.SUPPLEMENTARY NOTES

12a.DISTRIBUTION/AVAILABILITY STATEMENT

Approved for public release; distribution is unlimited.

12b.DISTRIBUTION CODE

13.ABSTRACT (Maximum 200 words)

New training facilities have been proposed for construction at the Fort Knox Northern Training Complex. These facilities include a digital training range and a complex of drop/landing zones and a maneuver area. During review of an Environmental Assessment, concerns about sediment erosion and adverse water quality impacts from the construction and project were expressed. Assessments of existing water quality data and the potential for sediment erosion were conducted to address potential impacts. Water quality data collected from 1995 to 1998 near the study area at the two major rivers, onsite data collected for discharge permit monitoring, data retrieved from the U.S. Environmental Protection Agency Storage and Retrieval system (STORET), and real-time discharge data were available for assessing existing conditions. Material loading was estimated using water quality and discharge data. Sediment yield for the preproject and postproject conditions for each alternative was conducted using the Revised Universal Soil Loss Equation, soil characteristics, and terrain slope developed from digital terrain elevation data. Water quality constituents generally fell within acceptable concentration ranges although total phosphorus concentrations were well above concentration guidelines used for lakes and reservoirs (0.02 mg L⁻¹), and elevated concentrations of solids, nutrients, and fecal coliform were most commonly observed with runoff events. Loading estimates indicated that sediment loads in the Salt River were about four times higher than in the Rolling Fork River.

(Continued)

14.SUBJECT TERMS

Fort Knox Loading

Salt River

Sediment erosion

Water quality

15.NUMBER OF PAGES

52

16.PRICE CODE

17.SECURITY CLASSIFICATION

OF REPORT

18.SECURITY CLASSIFICATION OF THIS PAGE

19.SECURITY CLASSIFICATION **OF ABSTRACT**

20.LIMITATION OF ABSTRACT

UNCLASSIFIED

UNCLASSIFIED

Standard Form 298 (Rev. 2-89) Prescribed by ANSI Std. Z39-18 298-102

13. (Concluded).

Sediment yield estimates were highest for the construction period but accounted for less than 0.2 percent of the annual load from each training area alternative to the corresponding receiving stream using preproject and postproject estimates. During construction, sediment yield estimates accounted for 4-10 percent of the annual load at most sites and near 20-40 percent at three sites, when no erosion control measures were considered, and provided a worst-case scenario. Actual loads were anticipated to be lower with the implementation of best management practices.